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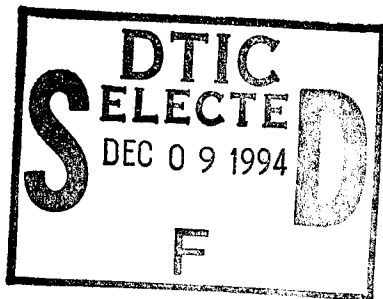
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NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

DESIGN OF A DIGITAL INTERFEROMETRIC DEMODULATOR

By

David William Brenner

September, 1994

Thesis Advisor:

Robert M. Keolian

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DESIGN OF A DIGITAL INTERFEROMETRIC DEMODULATOR

by

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Submitted in partial fulfillment
of the requirements for the degrees of

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ABSTRACT

This thesis investigates the design of a digital fiber-optic interferometric demodulator based upon a passive symmetric combination of signals produced by an interferometer terminated with a 3x3 optical coupler. The demodulator was implemented using a digital signal processing (DSP) board based upon a TMS320C31 DSP processor. The demodulator was tested using signals produced by a set of interferometric simulators which used an analog AD639 trigonometric chip. A goal of this thesis was to demonstrate an improved noise floor at low frequencies as compared with a similar analog implementation.

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I. INTRODUCTION

A. MOTIVATION

The motivation for this work is in support of the fiber optic hydrophone research being conducted at the Naval Postgraduate School. Push-pull fiber-optic hydrophones that have been designed and built by Garrett, Brown and associates at the Naval Postgraduate School offer very large acoustic sensitivities [Refs 1, 2, 3, 4 and 5]. This has offered the potential to develop acoustic sensor systems with wide dynamic ranges and high sensitivity. Various demodulation schemes are feasible for use with these interferometric sensors [Ref 6]. In particular, Cameron [Ref 7], has demonstrated an approach which terminates a Mach-Zehnder interferometer with a 3x3 optical coupler as shown in Figure 1.1. By using all three optical outputs and a passive symmetric demodulation scheme developed at the Naval Postgraduate School, he demonstrated superior results over other passive homodyne implementations. The algorithm is shown in block diagram form in Figure 1.2, below. Cameron constructed an interferometric demodulator based on the passive symmetric algorithm using analog electronics. With such, he was able to achieve a dynamic range of 115 dB @ 600 Hz in a one Hertz bandwidth with no more than 4% Total Harmonic Distortion (THD) [Ref 7:p 252]. The minimum detectable signal at that same frequency was 220 μ radians/ $\sqrt{\text{Hz}}$. Also Brown, et al., [Ref 8] quote comparable performance using a similar analog symmetric demodulator. They also note that both the minimum detectable signal (noise floor) and maximum tolerable signal increase as the acoustic frequency decreases.

At low frequencies, the analog electronic version of the symmetric demodulator suffered from excessive noise. When comparing the relative importance of noise contributions from various stages of a circuit, it is advantageous to refer the noise to a common spot in the circuit, for instance the input. This is done by dividing the noise injected at a stage by the accumulated gain of all the previous stages. The excessive low frequency noise was a consequence of the analog multiplier stage which follows the differentiators (refer ahead to Figure 1.2). A differentiator has gain which is proportional to frequency, going to zero at dc. Therefore, any noise in the multipliers at low

frequencies, will be of great importance; the noise power will diverge at dc as one over the frequency squared. The analog multipliers available for use in the analog symmetric demodulator were not particularly quiet. They had noise levels which were roughly equivalent to 16 bit noise in digital systems. However, the problem should be dramatically reduced if the symmetric demodulation can be implemented on a high speed Digital Signal Processor (DSP), where multiplication can be performed with 32 bit or better precision. For this reason it is hoped that a digital implementation will perform better than the analog version, and not have the dynamic range at low frequencies limited by excessive noise. McGinnis [Ref 9] investigated the use of digital algorithms to implement the symmetric demodulation scheme. He successfully programmed the algorithm in the LabVIEW™ programming language, and was able to demonstrate increased performance over the analog implementation (133 dB dynamic range @ 1 kHz 4% THD using a 51.2 kHz sampling rate).

B. GOAL

The goal of the thesis was to design, implement and test a digital fiber-optic interferometric demodulator using the passive symmetric demodulation scheme. Ultimately, a stand alone digital demodulator was to be built for use in the field. The performance of the demodulator was to be tested and compared against the analog version of the symmetric demodulator and the computer simulation conducted by McGinnis.

C. BACKGROUND

1. Interferometric Sensors

Interferometric sensors developed at the Naval Postgraduate School for sensing acoustic fields have been mostly based on the Mach-Zehnder two-beam interferometer, as illustrated in Figure 1.1. The sensor is comprised of a low power semiconductor laser which illuminates one leg of a 2x2 optical coupler. The output of the optical 2x2 coupler comprises the two legs of the Mach-Zehnder interferometer. Each leg is strained differentially by the field to be measured so that the two legs operate in a push-pull manner. The optical path length changes in the two legs cause interference in the 3x3 optical coupler whose output can be fed to photo diodes for detection and demodulation.

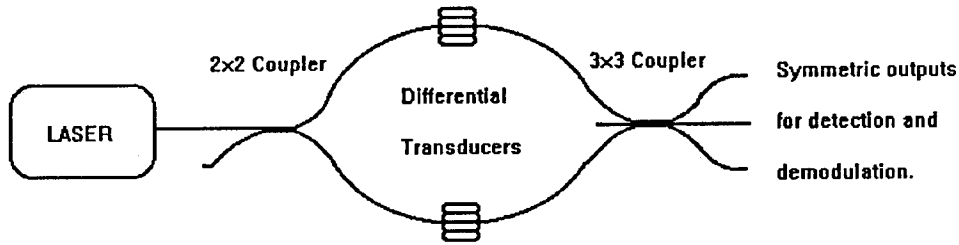


Figure 1.1. Schematic Diagram of a Fiber Optic Mach-Zehnder Interferometric Sensor

An ideal 3x3-coupler provides three signals of equal amplitude, each with a relative phase difference of 120° . The light intensities of each output leg from the 3x3-coupler are:

$$a = A + B \cos [\phi(t)], \quad (1.1)$$

$$b = A + B \cos [\phi(t) + 120^\circ], \quad (1.2)$$

$$c = A + B \cos [\phi(t) + 240^\circ], \quad (1.3)$$

where A is the average value of the optical intensity emitted by the optical fibers and B is the peak deviation in optical intensity from the average value A . The signal of interest, $\phi(t)$ is assumed to be time harmonic:

$$\phi(t) = \sin(\omega t) + \phi_{\text{drift}}(t). \quad (1.4)$$

The $\phi_{\text{drift}}(t)$ term accounts for the phase fluctuations due to environmental effects (hydrostatic pressure fluctuations and temperature changes) plus the static phase shift due to the physical differences in the two optical path lengths. These fluctuations are assumed to be slowly varying in comparison to the signal of interest and are therefore normally ignored. A theoretical plot of a 3x3 coupler output with constant A and B is shown in Figure 1.3. The three wave forms have been displaced from one another for clarity.

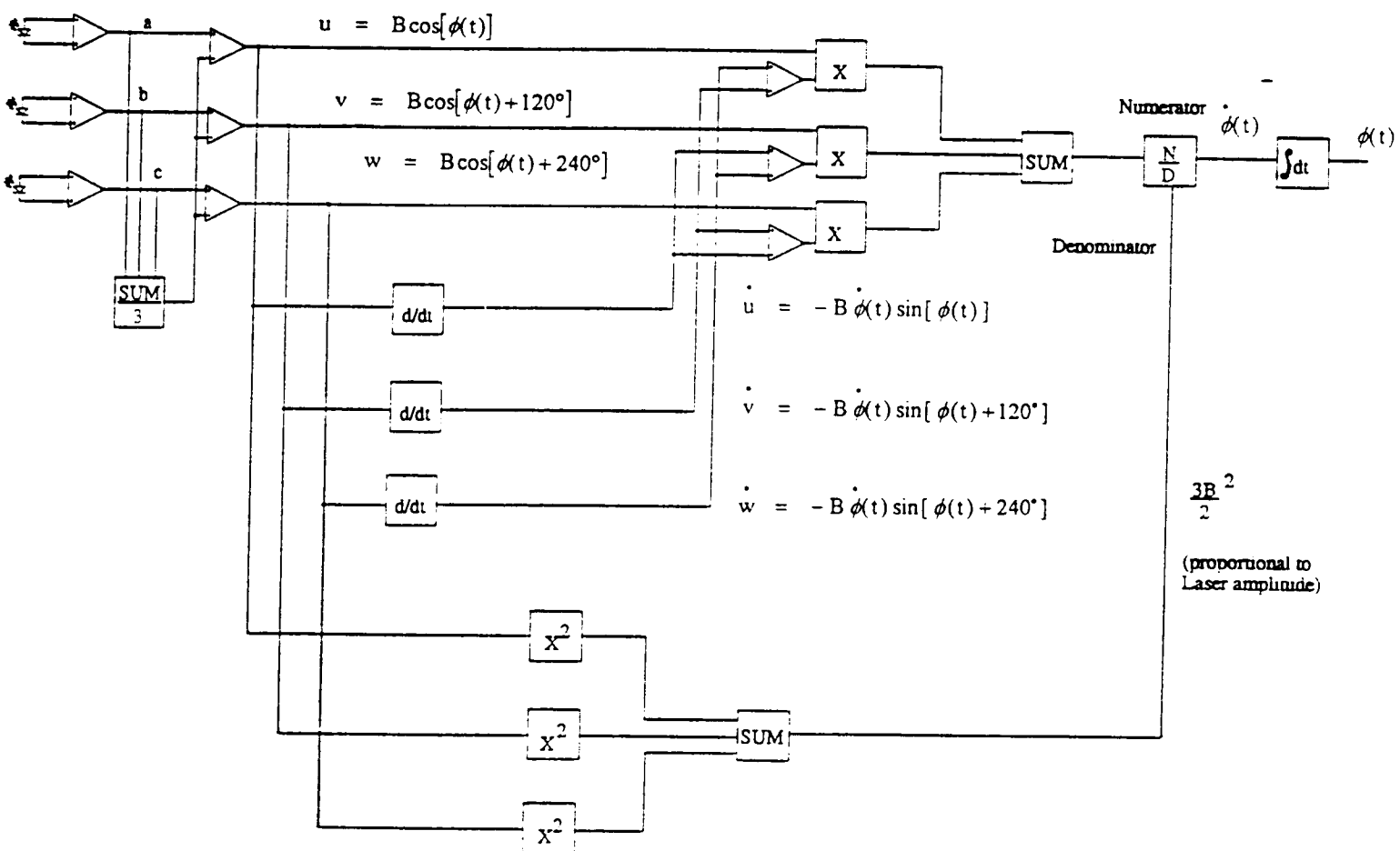


Figure 1.2 Block Diagram of the Symmetric Demodulation Algorithm.

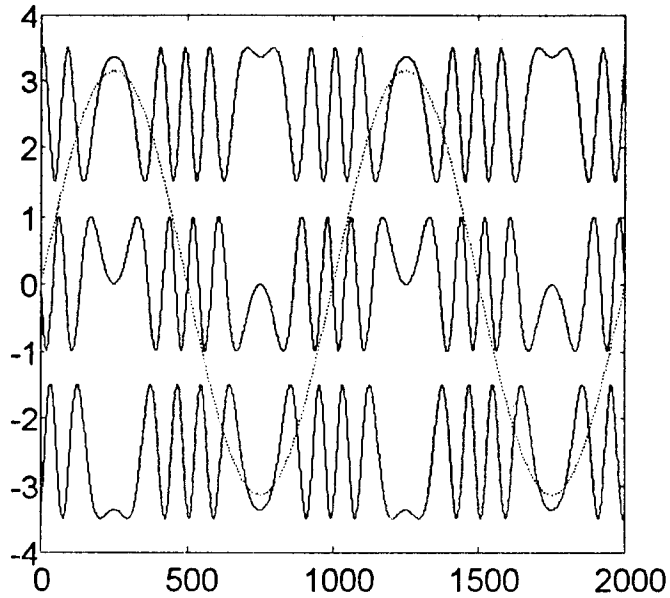


Figure 1.3 Theoretical Plot of 3x3 Coupler Output. Wave Forms a, b and c (solid lines) for an Input Signal (dotted line) which Produced 4 pi Radians of Optical Phase Shift in the Interferometer. The Wave Forms a, b and c have been Displaced from one another for Clarity.

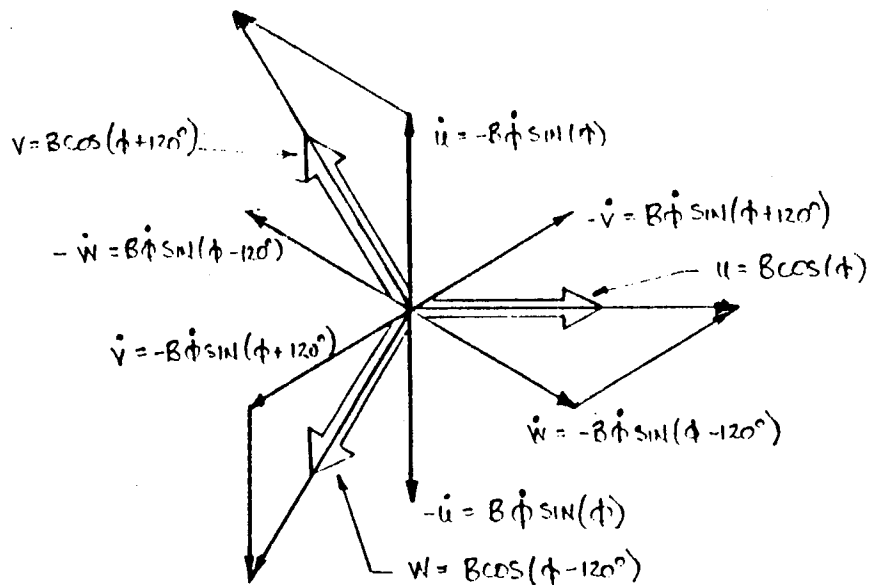


Figure 1.4 Phasor Diagram of Symmetric Demodulation Signals.

2. Symmetric Demodulation

The symmetric demodulation algorithm is based upon the following expression:

$$\phi(t) \propto \int \frac{u(\dot{v} - \dot{w}) + v(\dot{w} - \dot{u}) + w(\dot{u} - \dot{v})}{(u^2 + v^2 + w^2)} dt, \quad (1.5)$$

where $\phi(t)$ is the signal of interest to be recovered and the dots above variables indicates a time derivative.

The output intensity of each leg of the interferometer is as previously defined:

$$a = A + B \cos[\phi(t)], \quad (1.6)$$

with similar expressions for b and c . After photo detection and amplification, the three symmetric voltages are summed and scaled by a factor of $-1/3$ thereby producing an estimate of the average signal level. This average dc content is then subtracted from each of the interferometric voltage signals leaving only AC fluctuations about a bias of zero volts. The interferometric signals, with the average dc component removed are now denoted by u , v and w where

$$\begin{aligned} u &= B \cos[\phi(t)]; \\ v &= B \cos[\phi(t) + 120^\circ]; \text{ and} \\ w &= B \cos[\phi(t) + 240^\circ]. \end{aligned} \quad (1.7)$$

The three signals u , v and w are then differentiated to produce the derivative signals

$$\begin{aligned} \dot{u} &= -B \dot{\phi}(t) \sin[\phi(t)]; \\ \dot{v} &= -B \dot{\phi}(t) \sin[\phi(t) + 120^\circ]; \text{ and} \\ \dot{w} &= -B \dot{\phi}(t) \sin[\phi(t) + 240^\circ]. \end{aligned} \quad (1.8)$$

Note that $\dot{\phi}(t)$ has come out of the arguments of the trigonometric functions. These three symmetric-interferometric signals are then cross multiplied by the difference of the "complimentary" derivatives to yield:

$$\begin{aligned}
u(\dot{v} - \dot{w}) &= B \cos(\phi(t)) \left[-B \dot{\phi}(t) \sin(\phi(t) + 120^\circ) + B \dot{\phi}(t) \sin(\phi(t) + 240^\circ) \right]; \\
v(\dot{w} - \dot{u}) &= B \cos(\phi(t) + 120^\circ) \left[-B \dot{\phi}(t) \sin(\phi(t) + 240^\circ) + B \dot{\phi}(t) \sin(\phi(t)) \right]; \text{ and } (1.9) \\
w(\dot{u} - \dot{v}) &= B \cos(\phi(t) + 240^\circ) \left[-B \dot{\phi}(t) \sin(\phi(t)) + B \dot{\phi}(t) \sin(\phi(t) + 120^\circ) \right].
\end{aligned}$$

Figure 1.4 shows a plot of the signal phasors for the above combination of signals.

It can be shown by trigonometric identities that equation (1.9) can be simplified to:

$$\begin{aligned}
u(\dot{w} - \dot{v}) &= \sqrt{3}B^2 \dot{\phi}(t) \cos^2(\phi(t)); \\
v(\dot{u} - \dot{w}) &= \sqrt{3}B^2 \dot{\phi}(t) \cos^2(\phi(t) + 120^\circ); \text{ and } (1.10) \\
w(\dot{v} - \dot{u}) &= \sqrt{3}B^2 \dot{\phi}(t) \cos^2(\phi(t) + 240^\circ).
\end{aligned}$$

By noting:

$$\cos^2(x) + \cos^2(x + 120^\circ) + \cos^2(x + 240^\circ) = \frac{3}{2}, \quad (1.11)$$

the sum of the three equations in (1.10) can be shown to result in:

$$\dot{\phi}(t)B^2 \left[\cos^2(\phi(t)) + \cos^2(\phi(t) + 120^\circ) + \cos^2(\phi(t) + 240^\circ) \right] = \frac{3}{2} \sqrt{3}B^2 \dot{\phi}(t). \quad (1.12)$$

The factor of B^2 varies as a function of laser intensity, temperature, and the polarization angle of the light in the fiber. This dependence is removed by summing the squares of u , v and w .

$$u^2 + v^2 + w^2 = \frac{3}{2} B^2. \quad (1.13)$$

This result is used as a normalizing division factor. The ratio of equation 1.12 to equation 1.13 is then integrated to produce $\phi(t)$.

II. DESIGN OF A SYMMETRIC DIGITAL DEMODULATOR

This chapter discusses the details of the construction of a digital symmetric demodulator based upon the algorithm described in chapter 1. Available for use during this thesis was an IBM AT PC, a digital signal processing (DSP) plug-in board, and an interferometric signal simulator. The DSP card, the PC31, was built by Innovation Integration of Moorepark, California. It is described in Appendix A. The heart of the PC31 is comprised of a TMS320C31 DSP processor [Ref 10], which can be operated with either 32 bit integer precision or full 32 bit floating point precision using extended precision registers. Its 60 nsec single instruction cycle provides 16.7 million instructions per second (MIPS), or 33.3 million floating point operations per second (MFLOPS). The PC31 plugs into any IBM PC expansion bus (ISA), and can be fully programmed using either the Texas Instruments TMS320 Floating-point DSP Optimizing C compiler [Ref 11], or the TMS320 Floating-point DSP Assembly Language Tools [Ref 12].

The Interferometric signal simulator is described in Appendix B. The simulator is capable of simulating interferometric signals with optical phase shifts from several hundred micro-radians to about 2 pi radians.

The symmetric demodulator design involves the following phases: Photo detection of the three optical outputs from a 3x3 coupler; conversion to voltage signals proportional to the light intensity; digitization of the input interferometric signals; digital differentiation, multiplication, division, and integration. For my design, I have assumed that the three optical interferometric signals, each 120° out of phase with each other, have been suitably detected and conditioned to provide analog voltages which are limited to 2.75 Volts peak-to-peak. I now turn my attention to a discussion of each stage of the designed digital demodulator.

A. INITIAL DEMODULATOR DESIGN

1. Signal Digitization.

The PC31 provides two independent channels for analog input. Digital conversion is via one Burr Brown DSP102 ADC chip [Ref 13]. The DSP102 is a two channel analog-to-digital converter, ADC, which can operate at up to 200 kHz sampling rates

using either a 16 or 18 bit conversion size. Analog full scale input is set at 5.50 volts peak-to-peak. The DSP102 communicates with the TMS320C31 via a serial peripheral data bus. This data bus can operate at a maximum of 8.33 MHz. The DSP102 is configured in the cascade mode. When strobed, it simultaneously converts both channels A and B using a 16 bit conversion word and transmits the concatenated 32 bits across the peripheral serial bus. To convert both channels and transmit the 32 bit result to the TMS320C31 requires 4.8 μ sec at the maximum possible transport rate of 8.33 MHz. Channel A data occupies the upper 16 bits and channel B data the lower 16 bits of the 32 bit word conversion word. Using 16 bit conversion sizes results in approximately 84 μ V peak quantization per bit, with an error of one half the least significant bit, or $\pm 42\mu$ V.

The first problem faced with the design of the demodulator was how to sample three input channels using only one DSP102. Fortunately the PC31 allowed for eight channels to be multiplexed on the A input of the DSP102. Therefore as part of the first design, two of the three interferometric wave forms would have to be digitized by multiplexing them on channel A of the DSP102. This was the easiest approach to sampling, without designing complicated external digitization circuitry. However, this would reduce the effective sampling rate and would not produce simultaneous samples. Using a multiplexed digitization scheme, sampling channels A first and then B and C together would reduce the maximum possible sampling frequency by a factor of two. This will limit the maximum acceptable fringe rate (optical phase shift in the interferometer times signal frequency) of the demodulator. At the maximum possible sampling rate of 200 kHz, the two conversions required to sample the three interferometric signals would require a minimum time of about 10 μ sec. This should allow sufficient time to process one complete pass of the demodulation algorithm.

2. Algorithm Considerations.

As a first design, it was decided to calculate the derivatives of the interferometric signals using the method of first difference. This was chosen for its simplicity in implementation and least amount of computational burden. Since the TMS320C31 can support both floating point and integer operations, it was decided to initially implement the algorithm using integer operations since the input to the algorithm would be a 16 bit signed integer from the analog to digital converter, and the output would ultimately be in integer form for taking power spectra. However, careful consideration of the various signal maximums and minimums would be required to avoid overflows.

The denominator term in the algorithm takes the sum of the squares of the three input interferometric wave forms, essentially measuring the total optical power. Three 16 bit signed integers squared and added together could cause overflow in a resulting 32 bit integer. Therefore, the denominator was scaled down by a factor of 2^{16} . Similarly, the output of one of the multipliers is also a 16 bit number squared. This gets added to two other multiplier outputs, resulting in a potential overflow in a 32 bit integer. Therefore, each output from the multipliers was scaled down by a factor of two. Since the denominator had been scaled by 2^{16} the result from the division of the numerator (sum of the three multiplier outputs) and the denominator would be an integer just larger than 2^{16} . The integration of $\phi(t)$, was implemented using a first order difference equation $y(n) = 0.99 * y(n-1) + x(n)$, where the initial decay constant was set to 0.99. The output from the integrator is proportional to the signal that produced the original optical phase shift in the interferometer.

With the initial design considerations outlined, it was decided to initially program the algorithm using a well known platform, the IBM PC. Therefore the demodulation algorithm was first written in Turbo C [Ref 14] and tested on an IBM PC. However, this testing only used computer generated interferometric wave forms. The algorithm was also programmed in MATLAB [Ref 15]. Here, testing was first conducted using computer generated interferometric wave forms as inputs and then using data samples from the interferometric simulators taken using the PC31 and multiplexed sampling. The results of these simulations are described below.

B. SIMULATION ON AN IBM PC USING TURBO C

The designed demodulation algorithm was written in Turbo C and tested on an IBM PC. The demodulation program, TCDEMOC can be found in Appendix C. It was decided that by using a well known programming language and host computer, it would be easier to test and evaluate the demodulation algorithm from within a controlled environment. The MATLAB programming environment was used to display output from the TCDEMOC program. The MATLAB script file, PLOTDAT.M, used to display the data, is also included in Appendix C. The interferometric wave forms were generated by the TCDEMOC program and then demodulated using the algorithm discussed above.

Figures 2.1 - 2.4 show the various signals at different stages throughout the demodulation process. Computer generated interferometric waveforms produced by a

single sinusoid at 1/128th the sampling frequency with an amplitude which caused pi radians of optical phase shift in the interferometer were used as input for the demodulation algorithm. The simulated interferometric signals were created at full quantization of $\pm 2^{15}$. Figure 2.1 shows a plot of 200 samples of the computer generated interferometric input signals for full 16 bit quantization (± 32768). Figure 2.2 shows three plots of the derivatives of each input signal after the dc bias has been removed. The derivatives were calculated using a first difference approach. From the plots it can be seen that the maximum range for the derivative signals is ± 5000 for this particular input optical phase shift of pi radians. Figure 2.3 shows a plot of the first 500 samples of the numerator (left) and denominator (right) output from the demodulation algorithm. The numerator signal is proportional to $\dot{\phi}(t)$, which is the derivative of the signal of interest. Notice that it has been represented as 32 bit integer ($\pm 2.147 \times 10^9$). The denominator term, which is an estimate of the input laser power, is used to compensate for variations in the input signal caused by laser fluctuations. It is calculated by summing the squares of the signals u, v, and w and has been scaled down to accommodate a 16 bit representation. Notice the quantization noise associated with this scaling. The denominator fluctuates between 2.3435 and 2.3437, 2 bits of quantization noise, about 160 μV at full scale. Finally Figure 2.4 displays the output of the algorithm. This signal is from the digital integrator, a simple difference equation $y(n) = 0.99y(n-1) + x(n)$. Since this program only ran for just over 1000 samples the integrator decay is quite noticeable. The transients present at the first of the output are due to improper algorithm initialization.

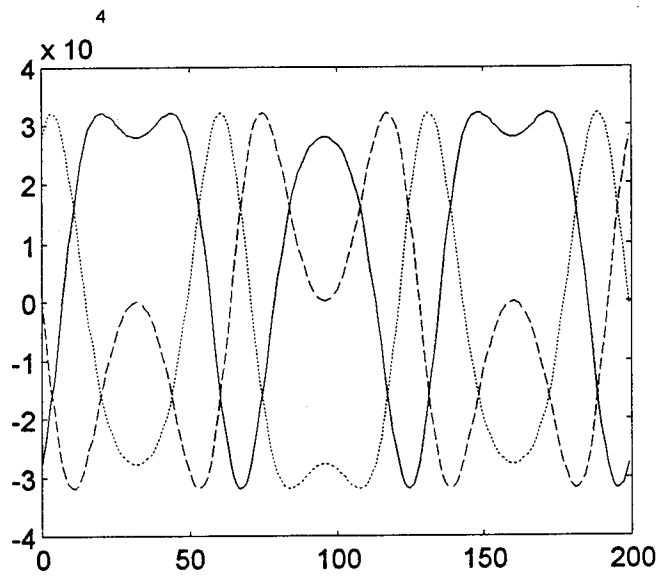


Figure 2.1 Input Interferometric Signals at Full Quantization. Signal a (solid line) Signal b (large dotted line) and Signal c (small dotted line).

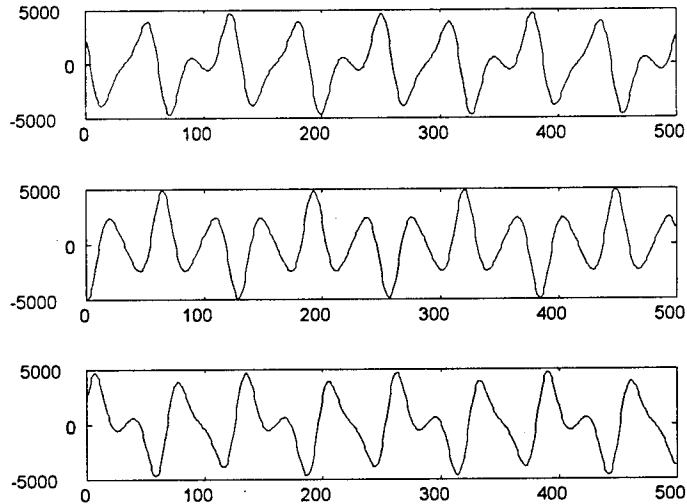


Figure 2.2 Derivatives of the Interferometric Inputs after the dc Component has been removed. Derivative of Signal u (top) Derivative of Signal v (middle), and Derivative of Signal w (bottom).

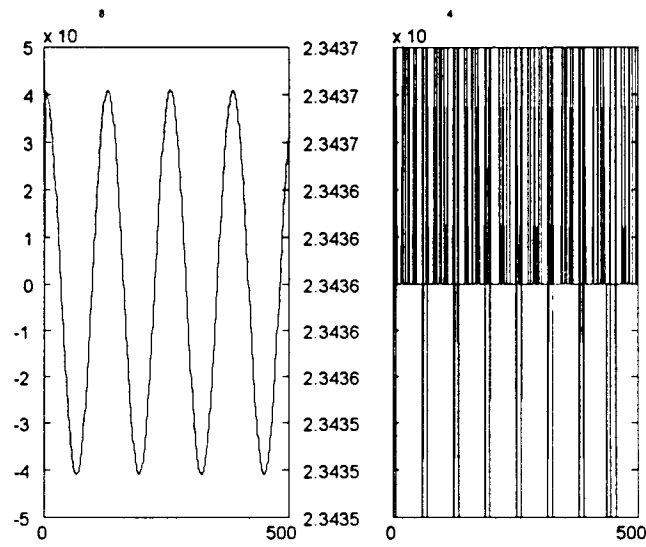


Figure 2.3 Output from the Numerator Calculations (left) and Output from the Denominator Calculations (right).

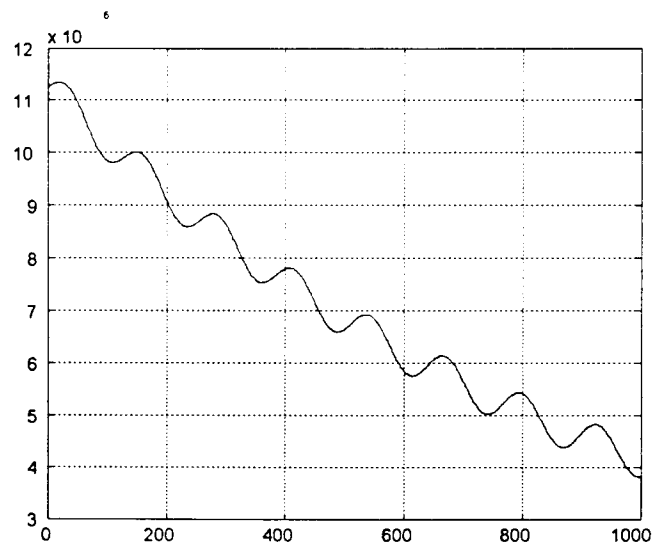


Figure 2.4 Demodulation Output which is Proportional to $\phi(t)$

The next set of Figures, 2.5 - 2.8, were again produced using the Turbo C demodulation program, TCDEMOD.C and MATLAB script file PLOTDAT.M. This time the program demodulated 10,000 points of computer generated interferometric data. The input signals and the last 2048 points of the output signal were stored and used for plotting in MATLAB. Figure 2.5 shows 200 points of the simulated interferometric wave forms for an input sinusoid at a frequency of $1/128$ that of the sampling frequency and an amplitude which would generate 10 radians of optical phase shift in an interferometer. Figure 2.6 shows plots of the resulting output from the demodulation process and its resulting power spectrum. Since only the last 2048 of the 10,000 output samples generated were plotted, the initial transients in the integrator have decayed and are not present in the output. The power spectrum plot was produced using the PSD.M script file from MATLAB's signal processing toolbox, version 3.1. The DFT size was 2048 points and a Hanning window of the same size was used to window the data. Notice that the signal has no dc present and it is outside the range of 16 bit quantization. The frequency of the signal is at 781.3 Hz, $1/128$ of 100 kHz sampling rate. The signal-to-noise ratio (SNR) is 140.6 dB, the peak output occurring at 114.8 dB. Notice the low distortion present. For a given frequency, as the optical phase shift in the interferometer increases, a result of an increase in the measured acoustic field, the distortion of the output increases. The next two Figures show this effect. Figure 2.7 shows a plot of the interferometric wave forms generated for an input sinusoid, again at a frequency of $1/128$ of the sample frequency, f_s , but at a much greater acoustic amplitude (50 radians optical phase shift produced in the interferometer). Figure 2.8 shows a plot of the output of the demodulator and a plot of its power spectrum. The effective fringe rate (optical phase shift times signal frequency) is now 39,000 fringes per second. Notice however that even at large distortion levels the output signal still resembles a sinusoid and may still be reasonably detected.

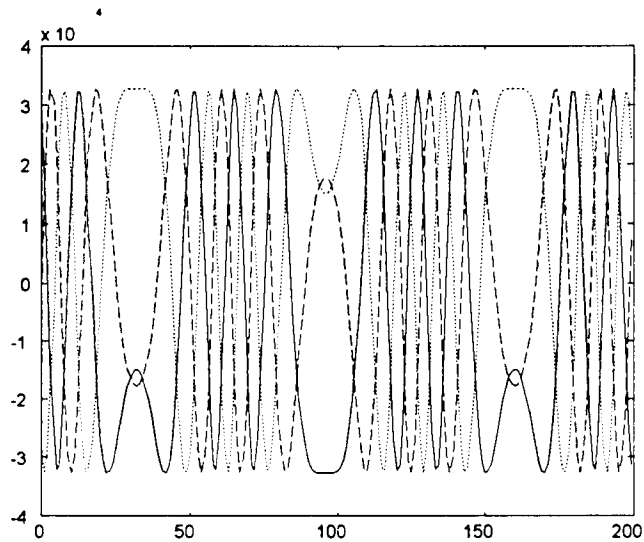


Figure 2.5 Computer Generated Interferometric Signals. The Input Signal is a Sinusoid at $1/128$ of the Sample Frequency, f_s with an Amplitude which Generated 10 Radians of Optical Phase Shift in the Interferometer.

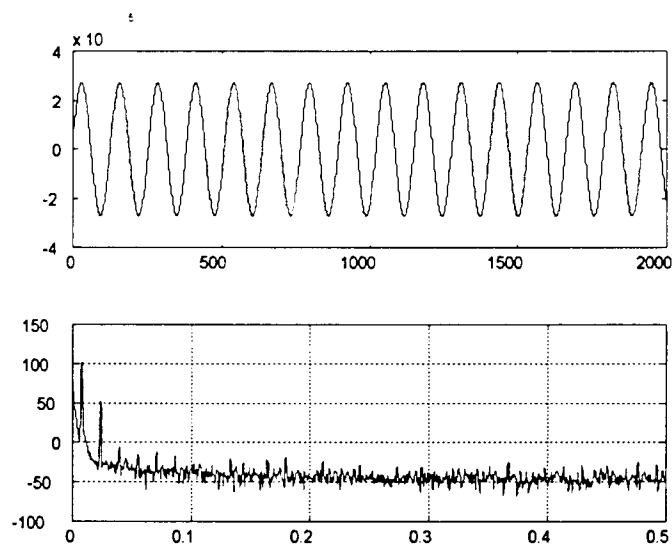


Figure 2.6 2000 Points of the Demodulator Output (top), and its Power Spectral Density Plotted in dB's (bottom).

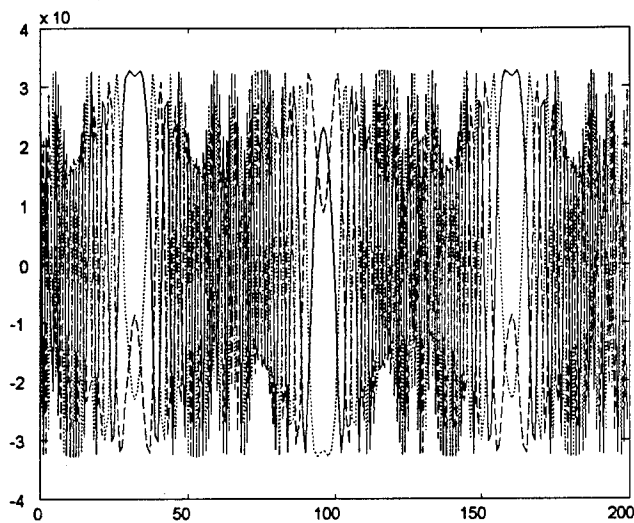


Figure 2.7 Input Interferometric Wave Forms for a Sinusoidal Input at $1/128$ the Sample Frequency, f_s and an Amplitude which Generated 100 Radians of Optical Phase Shift in the Interferometer.

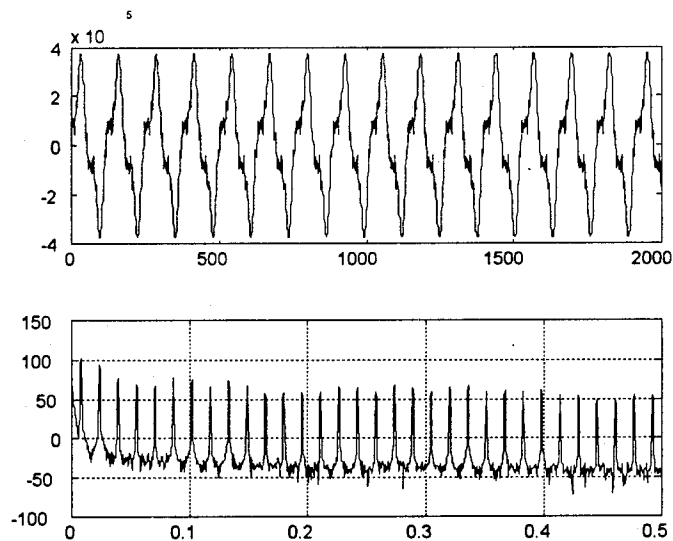


Figure 2.8 2000 Points of the Demodulator Output (top) and its Power Spectral Density Plotted in dB's (bottom).

C. SIMULATION USING MATLAB

It was decided to also simulate the demodulation algorithm in MATLAB. MATLAB offers a very easy programming environment where signals and noise can be readily simulated, processed and displayed. It offers the ideal environment for investigating the behaviour of the algorithm. MATLAB uses floating point arithmetic for its internal calculations, but output data can be rounded or fixed to the nearest integer. The script file, DEMOD.M, written for the MATLAB simulation can be found in Appendix C.

Figures 2.9 - 2.13 display various output wave forms from the demodulation process. Figure 2.9 is a plot of the MATLAB generated simulated interferometric signals. The input signal was a sinusoid at 600 Hz with an acoustic amplitude which resulted in π radians of optical phase shift in the interferometer. The simulated signals had a dc offset of 0.5 Volts peak and quantization amplitude equivalent to 2^{14} . Figure 2.10 is a plot of the derivatives of the three interferometric signals u , v and w after the dc component has been removed. The upper plot shows \dot{u} ; \dot{v} is plotted in the middle plot and \dot{w} is plotted in the bottom. The plots of the derivatives closely match those shown for the Turbo C program. Figure 2.11 shows plots of the outputs from the three multiplier stages. The top plot shows the output multiplication of signal u with the complementary derivatives $(\dot{w} - \dot{v})$, the middle plot shows the output from the multiplication of v with $(\dot{u} - \dot{w})$, and the bottom plot displays the output from the multiplication of w with $(\dot{v} - \dot{u})$. Figure 2.12 displays plots of the numerator and denominator signals. Notice how the denominator once again has one bit of quantization noise. This is a result of fixing the floating point value output from MATLAB. The denominator is very close to a constant value for this simulation. However, the program allows for simulation of slowly fluctuating laser inputs. Notice also that at this level of optical phase shift the numerator term has not yet exceeded 32 bit integer quantization limit. Figure 2.13 shows the output signal from the demodulation process and its power spectral density. The output looks very clean, and indeed has very little distortion as indicated by the power spectrum. Notice that the output from this MATLAB simulation is less distorted than the output from the Turbo C simulations. The demodulation algorithm was extensively simulated using MATLAB, over a wide range of frequency ratios (input frequency divided by sampling frequency), an input optical phase shifts. Several observations were noted. First, the numerator overflows a 32 bit signed representation using integer arithmetic for large fringe rates

(fringe rates greater than 100). Therefore the components making up the numerator will have to be scaled by a factor of one half. This will be sufficient to avoid any overflow. Secondly, at small optical phase shifts, 100's of micro radians, the demodulator sensitivity will be determined by the signal derivatives which under flow 16 bit quantization first. With these discoveries in mind it was now time to implement the algorithm on the PC31.

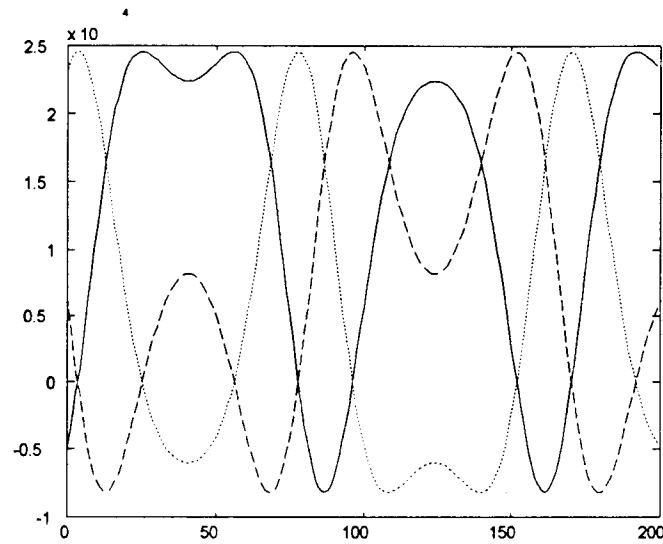


Figure 2.9 MATLAB Generated Interferometric Wave Forms. Signal a (dotted line), Signal b (dashed line) and Signal c (solid line).

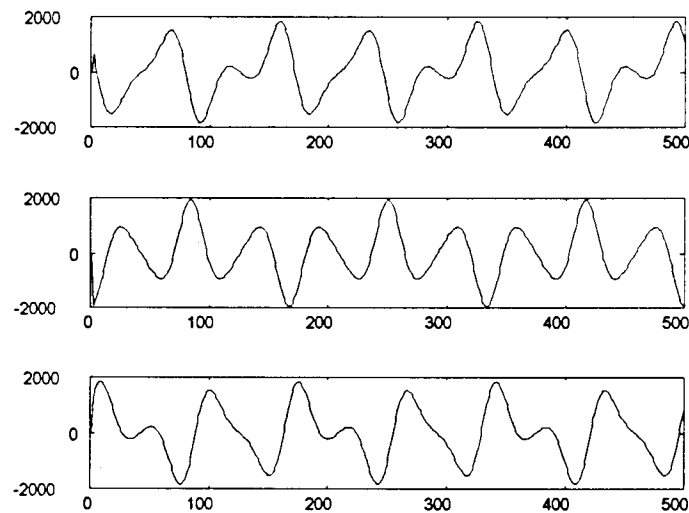


Figure 2.10 Derivatives of the Interferometric Signals with the dc Component Removed. Derivative of signal u (Top), Derivative of signal v (Center), and Derivative of Signal w (Bottom).

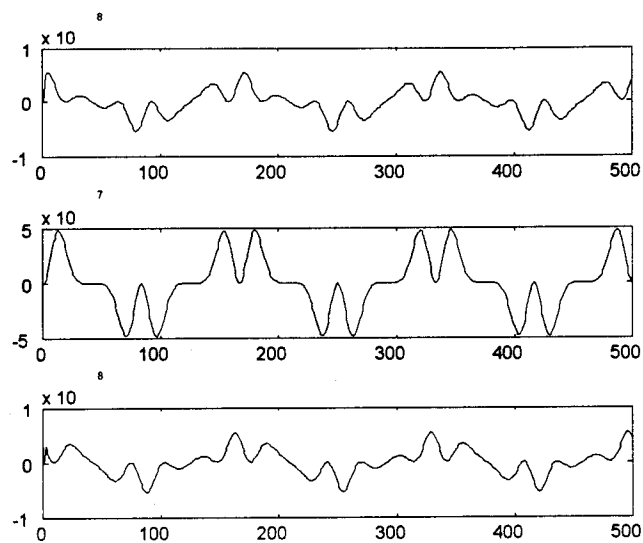


Figure 2.11 Outputs from the Three Multiplier Stages. (Top) $u(\dot{w} - \dot{v})$, (Center) $v(\dot{u} - \dot{w})$, and (Bottom) $w(\dot{v} - \dot{u})$.

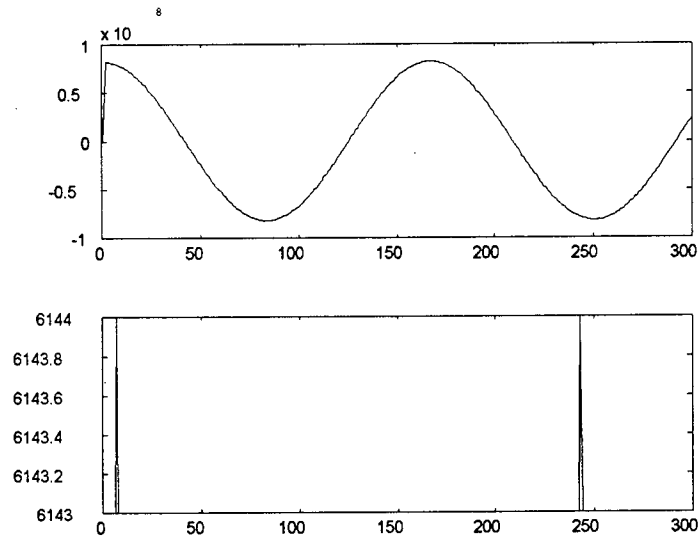


Figure 2.12 Numerator signal (Upper plot). Denominator signal (Lower plot).

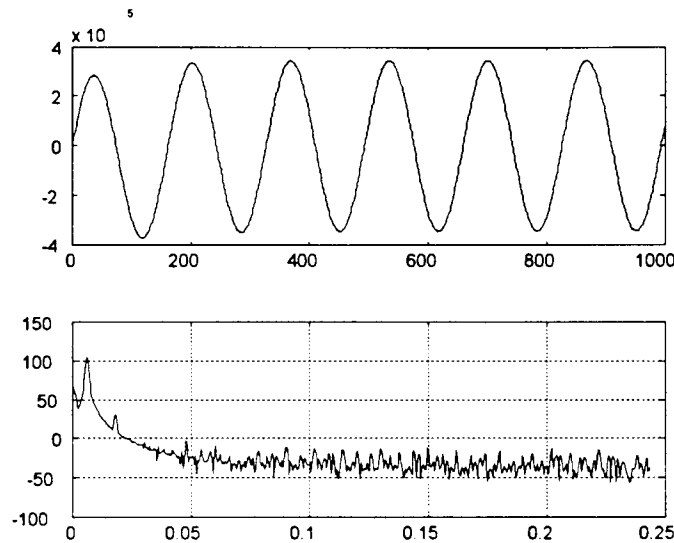


Figure 2.13 Demodulator Output (Upper plot) and its Power Spectral Density Plotted in dB's vs. Nyquist Frequency (Lower plot).

D. PROGRAMMING THE PC31

Once the algorithm had been successfully programmed and tested in MATLAB, it was time to consider an implementation on the PC31 DSP board. I initially decided to program the demodulation algorithm in C using the TMS320 optimizing C compiler. The program titled TMSDEMOC.C can be found in Appendix C. The most challenging part of implementing the demodulator design on the PC31 was in choosing the method used to sample the three interferometric signals.

1. TMS320 Optimizing C Compiler Programs

The DSP102 analog-to-digital converter (ADC) can be strobed to start a conversion by either writing to a memory location, or by jumping one of three different programmable clocks on the PC31 board to the convert pin of the DSP102. Once a conversion is complete (analog-to-digital conversion plus transport of 32 bits along the serial port), the TMS320C31's internal serial port generates an interrupt signal when its receive buffer is full. This interrupt signal can be used to interrupt the CPU at the end of a conversion. It can also be masked, in which case the program must poll the serial port and wait for the conversion to complete. I initially decided to run the conversion process using a polling approach. The conversion process of the multiplexed input line IN0 starts

when a dummy store was made to the memory location decoded for the ADC. After receiving the convert command the DSP102's internal hold circuitry keeps the inputs constant while the conversion is in process. This allows the inputs to the DSP102 to be changed immediately after a convert command has been given. Therefore while the conversion is in process the multiplexer channel is switched to another input, IN1. This gives the multiplexer sufficient time to settle (the analog multiplexer requires 1 μ sec for its output to settle to within 0.1% of true value. Waiting 3.5 μ sec increases the accuracy to 0.01%). After 4.8 μ sec, the converted data is received at the serial port and can be read by the program. The first conversion made by the DSP102 is not valid and must be discarded. The next conversion represents the first data sample. Once the data is read, a new conversion can be signaled with a write to the ADC's memory location and the multiplexer can be switched back to channel IN0. The data read from the DSP102 is shifted to the right 16 bits, representing signal sample a, which is stored until all three signal samples are read. The program then waits for the next sample by polling the status of the serial port. Once the next conversion has been received it is read and the 32 bit conversion word is separated into sample b (upper 16 bits) and sample c (lower 16 bits). Once the three samples have been read the program enters the demodulation process. The denominator term, derivatives and numerator are calculated and used to compute the first output sample. This loop repeats itself until 4000 data samples have been computed.

Several C programs were written to test various aspects of the demodulation algorithm and to save other intermediate variables. The internal memory storage of the PC31 was limited to 26,600 32 bit words of storage for both program and data. Therefore not all intermediate data could be stored at one time. Once computed the data could be downloaded from the PC 31 for viewing and manipulation in MATLAB. Although the programs written in C and compiled using the TMS320 optimizing C compiler were successful in implementing the demodulation algorithm, the execution was not very fast and this limited the effective sampling rate. This was due in part to the optimizing C compilers usage of the TMS320C31 register set and the adherence to the TMS C function calling conventions. Also, the routines were slowed down because of the need to wait for ADC conversions while polling. The solution to the two problems was to switch to assembly language programming, instead of using the C compiler, and use serial port interrupts instead of polling. Use of interrupts would allow the demodulation routine

to continue with computations instead of having to poll the serial port for new ADC conversions.

2. TMS320 Assembler Programs

After several long months of learning the intricacies of the TMS320C31 addressing modes, I was ready to tackle the job of writing the demodulation algorithm in assembly language. I first wrote a simple assembly language routine to sample data presented to channels IN0 and IN1 of the multiplexer and input B of the DSP102. This program is called TST3.ASM and it is included in Appendix C. The program takes up to 8192 points of data from the three input channels. The DSP102 ADC is driven using internal timer clock number one (TCLK1) from the TMS320C31. The serial port interrupts the CPU when it has received the full conversion from the ADC. Input A to the DSP102 is multiplexed through channels IN0 and IN1 of the multiplexer. Interferometric signal a is connected to IN0 and interferometric signal b is connected to IN1. Interferometric signal c is connected directly to input B of the DSP102, which is not multiplexed. After initialization of the serial port, internal timer and program variables, the interrupts are enabled and the program waits in an infinite loop until interrupted. Data from signal a (upper 16 bits of first serial port read) is read and stored after the first interrupt. The data read from input B of the DSP102 is discarded. The multiplexer channel is then switched to channel IN1 and the routine waits for the next interrupt. Once interrupted, data from signal b (upper 16 bits) and signal c (lower 16 bits) are read and stored. This completes the sampling of the first three interferometric signals. The multiplexer is then switched back to channel IN0 and waits for the next interrupt in order to get the next set of samples. A data index pointer increments after collecting the three data samples. After taking 8192 samples the interrupts are disabled and the PC31 can be reset. The sampled data can then be downloaded to the host computer. This routine can be run at the maximum sampling frequency of 200 kHz. However, because of the need to multiplex the input data, the effective sampling rate for all three channels is reduced in half to 100 kHz.

Once the multiplexed data sampling routine, TST3.ASM had been written and tested, it was time to consider the implementation of the complete demodulation algorithm. Program TST5.ASM, shown in Appendix C, is the routine I developed to implement the demodulation algorithm on the PC31 using integer operations. This routine accepts three simulated interferometric signals a, b and c each 120° out of phase with each other. The outputs from the interferometric signal simulators are applied to IN0, IN1 and

input B on the DB37 analog connector on the back of the PC31. The algorithm digitizes this data and implements a symmetric demodulation of the input signals using integer operations. 8192 points of the denominator, numerator and output are computed and stored for downloading to the host computer. Several interesting statistics about the algorithms timing were clarified during the development of this routine. First, it takes about 540 nsec (9 instructions) from an interrupt occurring to the first instruction of the interrupt service routine. Secondly, the time required to read sample a after an interrupt has occurred, switch the multiplexer to channel IN1, store the data and return from the interrupt takes about 1.5 μ sec. Once the first data sample has been read, from the time the second interrupt is generated to the end of the demodulation process requires 10 μ sec. However, this time varies by as much as 1 μ sec. This is because of the integer division. Each integer division requires between 31 - 62 cycles to execute depending upon the amount of normalization needed. However, each floating point divide requires only a fixed 40 cycles to execute. The assembly language routines which implement these divisions were provided with the TMS320 development package.

Since using a floating point divide may be quicker in some cases than an integer divide, I decided to also implement the demodulation algorithm using floating point operations. Assembly language routine TST7.ASM implements the demodulation algorithm floating point operations on the PC31. This program is also included in Appendix C. Only minor changes were required to TST5.ASM to implement the algorithm in floating point. However, I had to be careful to use the 40 bit extended precision registers R0 - R7, which offer a full 32 bit mantissa field and an eight bit exponent field. Again 8192 points of the denominator, numerator and output are calculated and stored. Before the results are stored they are converted to 32 bit integers. This was required since the 40 bit extended precision registers cannot be fully stored in a 32 bit memory location. Also, 32 bit integers were required for downloading to MATLAB for analysis.

III. PERFORMANCE OF THE DIGITAL DEMODULATOR

The digital demodulator was tested using the analog interferometric signal simulators as the source for the interferometric wave forms. See Appendix A for a description of the signal simulators. Each simulator was set to output 3.0 volts peak-to-peak. This corresponded to the design input of 1.5 volts peak for each channel of the DSP102. The interferometric simulators were driven using a Stanford Research Systems, Model DS345 function generator which provided the source signal $\phi(t)$. The frequency and amplitude of the input source signal determine the frequency and optical phase shift of the interferometric waveforms. The static phase shift of each simulator was set such that each of the three outputs was 120° out of phase from each other. The testing of the demodulator proceeded in three phases. First, the DSP102 and the multiplexed sampling dynamics were tested for full scale voltage linearity, noise and offset. Secondly, the analog signal simulators were sampled to see how they compared to theoretical computer generated interferometric wave forms. Finally, the demodulator output was tested using several sinusoids at various amplitudes.

A. TESTING OF THE INPUT SAMPLING CIRCUITS.

First the DSP102's offset and gain adjustment were checked using the procedures outlined in the PC31 user's guide [Ref 16:p 40]. The program TST3.ASM, shown in Appendix C, was assembled using the TMS320 assembler and then downloaded to the PC31 to run the data collection program. The multiplexer and ADC were then tested using a single sinusoid applied to IN0, and IN1 of the multiplexer and channel B of the DSP102. A 600 Hz sinusoid was generated using a Stanford Research Systems Model DS345 function generator set to 2.0 volts r.m.s., the full scale voltage for the DSP102 inputs. The three channels were then sampled at 151.5 kHz for an effective multiplexed sampling rate of 75,757.6 Hz. Data was collected on the PC31 and then was downloaded to the PC for analysis using MATLAB.

1. Data for Full Scale Inputs

Figures 3.1 to 3.3 were generated using the MATLAB script file PLOTABC.M, included in Appendix C. The power spectral density estimates were calculated and plotted

using the program PSD.M from the signal processing toolbox, version 3.1. 8192 points were used for the DFT calculations and the data was windowed with a Hanning window of the same size. The Total Harmonic Distortion (THD) estimate was made using the fundamental and the first 10 harmonics. Figure 3.1 shows a plot of the data taken from channel IN0 of the multiplexer (upper plot). The power spectral density of channel IN0 and an estimate of the distortion present is shown in the lower plot. Figure 3.2 shows plots of data taken from channel IN1 of the multiplexer. Theoretically Figures 3.1 and 3.2 should be identical. Any differences between the two plots are due to the differences in the two multiplexer channels. As can be seen from the plots, both channels are very close to each other. Figure 3.3 shows data taken from channel B of the DSP102. In all three plots the 2.0 volts r.m.s. input produces close to full scale readings from all three channels. The signal generator used to generate the test sinusoid or the DSP102 has about 2% total harmonic distortion. This was the same function generator which was used to drive the three interferometric signal simulators.

2. Data for Inputs Grounded.

Next, IN0, IN1 and input B were grounded to the analog ground plane. Program TST3.ASM was downloaded to the PC31 and the three channels were sampled at an effective rate of 75,757.6 Hz. 8192 points of the sampled input were taken, stored and downloaded to the PC for plotting in MATLAB. The plots were generated using the script file PLOTABC.M, however, this time only 4096 points of the data were used for the power spectral density plots resulting in a bin width of 18.5 Hz. Using a 4096 point Hanning data window gave an equivalent noise bandwidth of 22.75 Hz [Ref 17] for the power spectrum plots. Figures 3.4 - 3.6 show plots of this grounded condition. Notice the noise on all three channels. It is digital in nature and has large fluctuations about zero. Figure 3.4 shows sampled data from channel IN0. The upper plot shows 500 points of the sampled data. Using the calculated standard deviation of 3.663 the noise for channel IN0 was calculated to be about 0.3 mV. Figure 3.4 shows plots of data taken from input IN1 to the multiplexer. Using the calculated standard deviation of the data, the noise for this channel was calculated to be also about 0.3 mV. Figure 3.6 shows plots of data taken from input B to the DSP102. Using the calculated standard deviation, the noise for this channel was calculated to be about 0.4 mV. Input B to the DSP102 is slightly more noisy than channel A. This can also be seen from Figure 3.6 where it is easy to see that the gain

setting for input B of the DSP102 is slightly higher than that of input A. Also, both channels are slightly offset from zero.

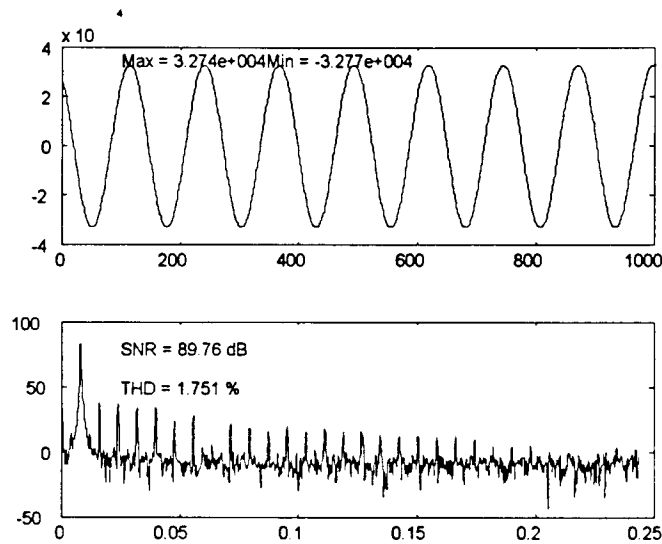


Figure 3.1 Plots of Full Scale Input to Multiplexed Channel IN0. Sampled Data Plotted as a Function of Magnitude and Sample Number (Upper plot). Power Spectrum of Input Plotted in dB's vs. Nyquist Frequency (Lower plot).

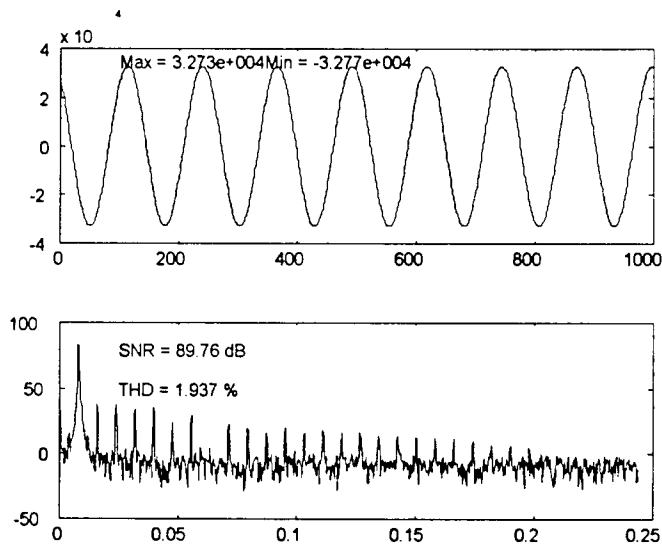


Figure 3.2 Plots of Full Scale Input to Multiplexed Channel IN1. Sampled Data as a Function of Sample Number and Magnitude (Upper plot). Power Spectrum of Input Data Plotted in dB's vs. Nyquist Frequency (Lower plot).

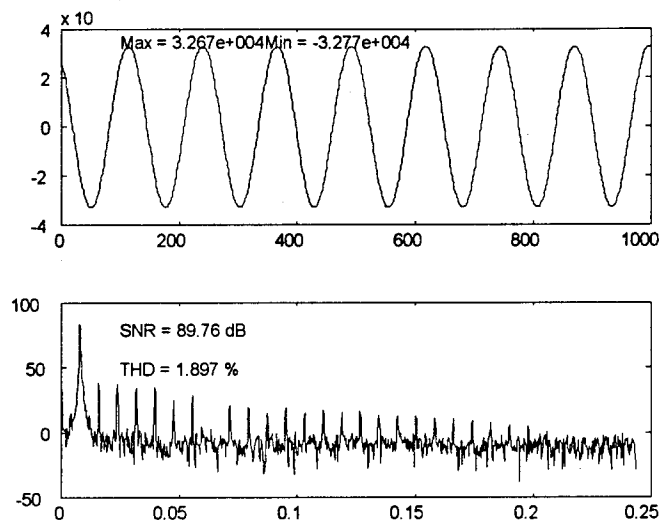


Figure 3.3 Plots of Full Scale Input to Input B of the DSP102. Sampled Data Plotted as a Function of Magnitude and Sample Number (Upper plot). Power Spectrum of the Sampled Data Plotted in dB's vs. Nyquist Frequency (Lower plot).

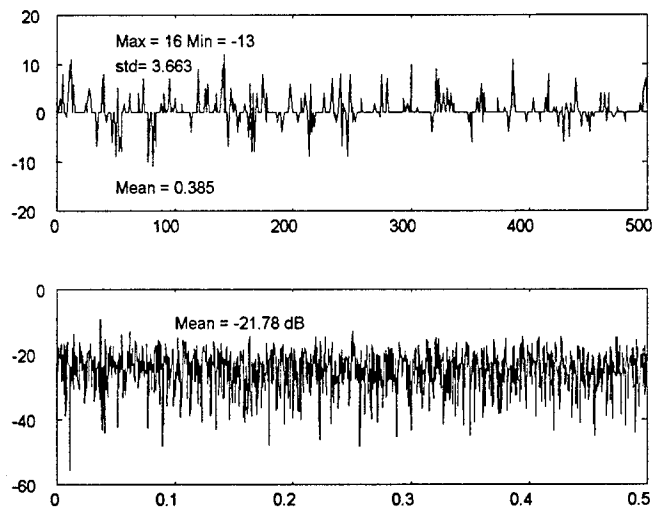


Figure 3.4 Plots of Channel IN0 of the Multiplexer for Grounded Input. First 500 Data Points of Sampled Input (Upper plot). Power Spectral Density of Channel IN0 Plotted in dB's vs. Nyquist Frequency (Lower plot).

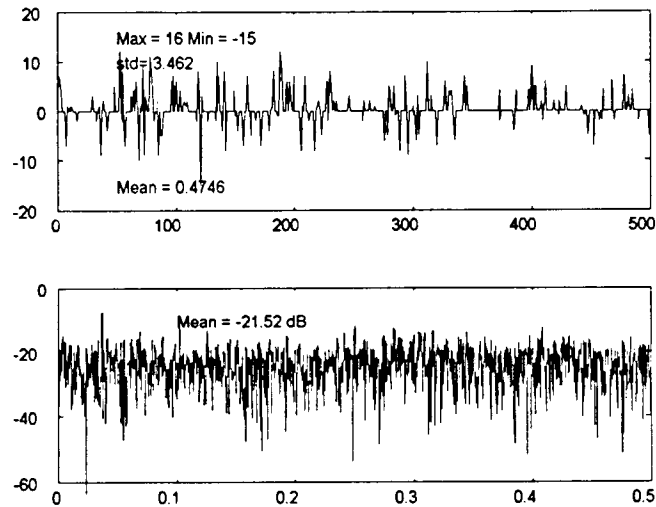


Figure 3.5 Plots of input IN1 of the multiplexer for Grounded Input. First 500 Data Points of Sampled Input IN1 (Upper plot). Power Spectral Density of Grounded Channel IN1 Plotted in dB's vs. Nyquist Frequency (Lower plot).

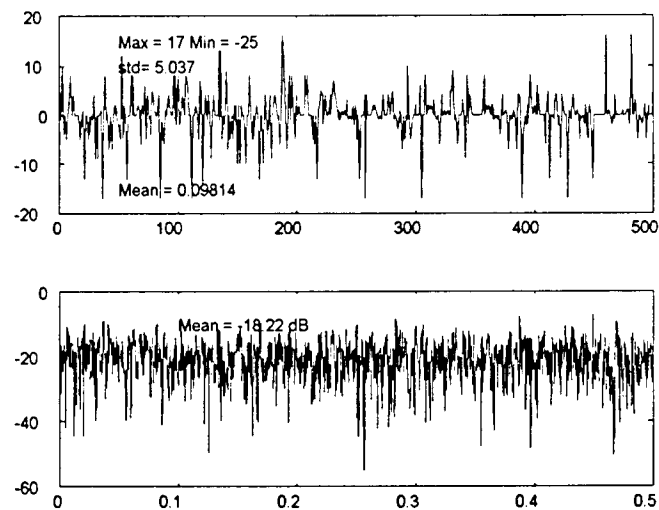


Figure 3.6 Plots of Input B to the DSP102 for Grounded Input. First 500 Data Points of Sampled Input (Upper plot). Power Spectral Density of Grounded Channel B Plotted in dB's vs. Nyquist Frequency (Lower plot).

B. SAMPLING OF THE INTERFEROMETRIC SIGNAL SIMULATORS

The next test was conducted using the interferometric signal simulators. The simulators were driven with a 1.0 kHz sinusoid at an amplitude of 1.0 Volt peak. This produced interferometric wave forms with about 1.0 radian of optical phase shift since the scale factor for the simulators was 0.933 rad/Volt (see Appendix B). The data was taken using program TST3.ASM set to sample the data at an effective sampling rate of 75,757.6 Hz. The output from the PC31 was downloaded, analyzed and plotted in MATLAB using the script file LDTST3.M. This program is included in Appendix C. The power spectral density plots of the interferometric channels were calculated with program PSD.M, using 2048 point DFTs and a Hanning data window of the same size. This gave an equivalent noise bandwidth of 45.5 Hz.

Figures 3.7 - 3.9, show plots of the sampled interferometric channels. Plot 3.7 is a plot of interferometric simulator #1 which was set to a static phase shift of -120° . This was applied to channel IN0 on the analog connector to the PC31. The top plot displays the sampled data while the bottom plot displays the power spectrum plotted in dB's vs. digital frequency f/fs . Figure 3.8 is a plot of interferometric simulator #2 set to a static phase shift of 0. It was connected to IN1 on the analog connector to the PC31. Figure 3.9 shows plots of interferometric simulator #3, set to a static phase shift of $+120^\circ$. It was connected to Input B of the DSP102. All three simulated wave forms produce spectrums which are typical for interferometric signals.

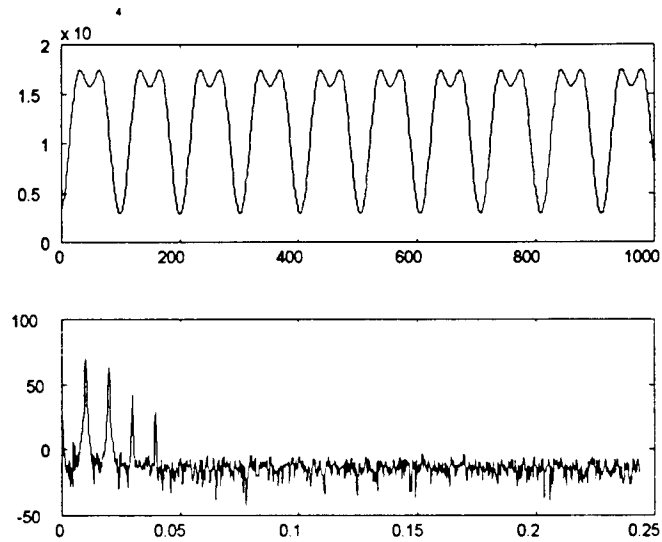


Figure 3.7 Plots of Interferometric Signal Simulator #1 Set to a Static Phase Shift of -120° , 1.0 kHz Input and 1.0 Radian of Optical Phase Shift. Multiplexed Channel IN0 Sampled at 75,757.6 Hz (Upper plot). Power Spectrum of Interferometric Signal Plotted in dB's vs. Nyquist Frequency (Lower plot).

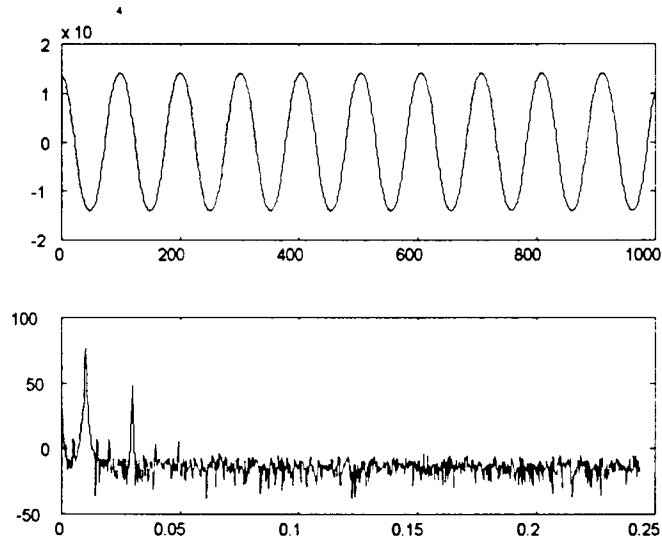


Figure 3.8 Plots of Interferometric Signal Simulator #2 Set to a Static Phase Shift of 0° 1.0 kHz Input and 1.0 Radian of Optical Phase Shift. Multiplexed Channel IN1 Sampled at 75,757.6 Hz (Upper plot). Power Spectrum of Interferometric Signal Plotted in dB's vs. Nyquist Frequency (Lower plot).

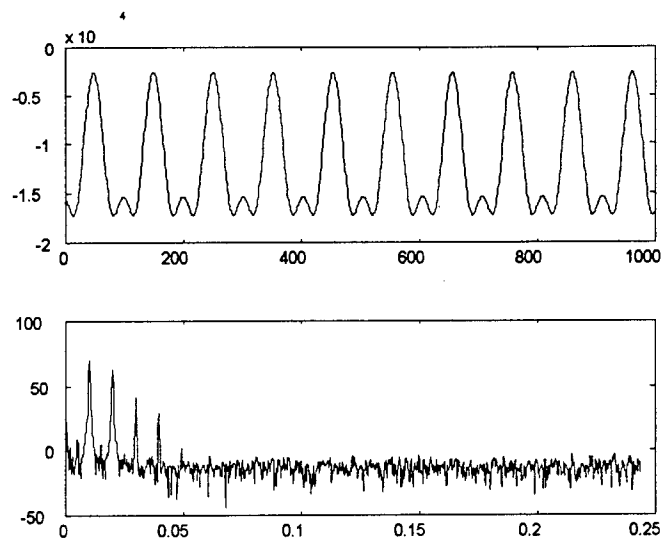


Figure 3.9 Plots of Interferometric Signal Simulator #3 Set to a Static Phase Shift of $+120^\circ$, 1.0 kHz Input and 1.0 Radian of Optical Phase Shift. Input B to DSP102 Sampled at 75,757.6 Hz (Upper plot). Power Spectrum of Interferometric Signal Plotted in dB's vs. Nyquist Frequency (Lower plot).

C. DIGITAL DEMODULATOR OUTPUT.

The two assembly language programs written to perform the digital demodulation, TST5.ASM (integer operations), and TST7.ASM (floating point operations), were tested. TST5.ASM was run at an effective sampling rate of 69,444.4 Hz, while TST7.ASM could be run a little faster at 75,757.6 Hz. Three interferometric signal simulators driven by the Stanford Research Systems DS345 function generator were used to simulate the interferometric wave forms for the demodulator.

1. Demodulator Response to Input Frequency Variations.

The demodulator response to frequency variation was tested by simulating interferometric signals at constant optical phase shift but at two separate frequencies of 600 and 1200 Hz. For program TST7.ASM using a sampling rate of 75,757.6 Hz the input frequencies were 0.0079 and 0.0158 times the sampling rate, fs. For program TST5.ASM using a sampling rate of 69,444.4 Hz, the input frequencies were 0.0086fs and 0.0173 times the sampling rate, fs. Interferometric wave forms with pi radians of optical phase shift were produced using the interferometric simulators. In each run, 8192 points of the denominator, numerator and output signals were calculated by the demodulation program and later downloaded to the PC. Plotting and analysis of the data was conducted in MATLAB using the script files LDTST5.M and LDTST7.M. Power spectrum estimates were plotted using MATLAB's PSD.M script file from the signal processing toolbox, version. 3.1. The data was windowed using a 4096 point Hanning window thereby producing an equivalent noise bandwidth of 22.75 Hz. The power spectral density plots were plotted in dB's versus Nyquist frequency. Figures 3.10 through 3.13, show demodulator output taken using the program TST5.ASM. Figures 3.14 through 3.17 show output taken using the program TST7.ASM. The estimates of the harmonic distortion were made using the fundamental and first ten harmonics. Both denominator plots in Figure 3.11 and 3.13 show variations due to the non-simultaneous sampling. The denominator term, an estimate which is proportional to the laser power, should be a constant since the simulated interferometric signals have no variation due to laser power fluctuations.

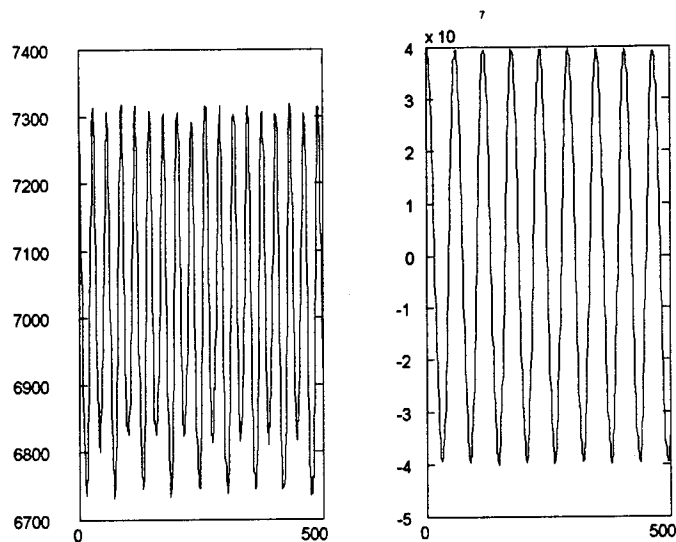


Figure 3.10 Denominator Divided by 2^{16} (Left plot) and Numerator (Right plot) Calculated Using Program TST5.ASM for Input Interferometric Signals of π Radians Optical Phase Shift at Frequency 0.0176fs.

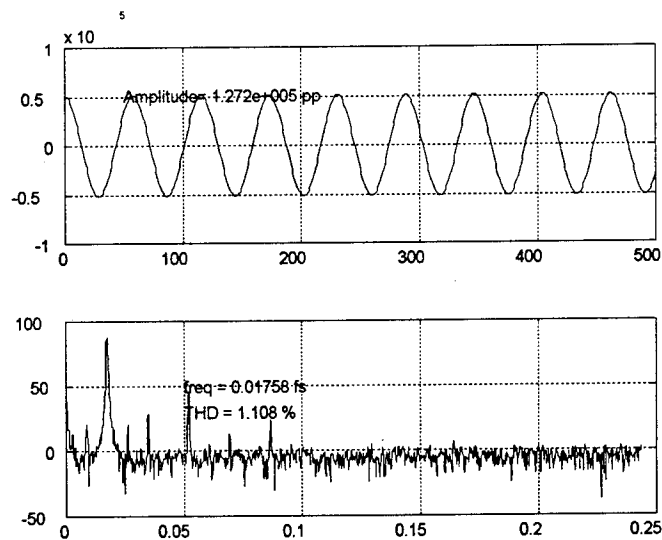


Figure 3.11 Demodulator Output for Interferometric Input of π Radians Optical Phase Shift at Frequency 0.0176fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

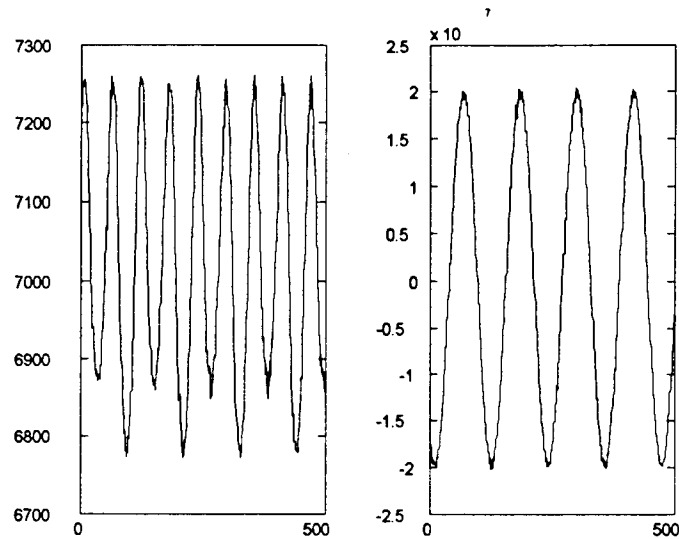


Figure 3.12 Denominator Divided by 2^{16} (Left plot) and Numerator (Right plot) Calculated Using Program TST5.ASM for Input Interferometric Signals of π Radians Optical Phase Shift at Frequency 0.0088fs.

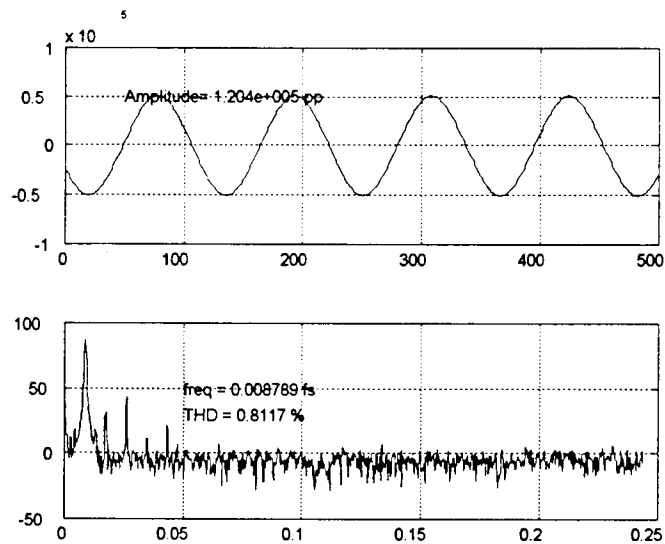


Figure 3.13 Demodulator Output for Interferometric Input of π Radians Optical Phase Shift at Frequency 0.0088fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

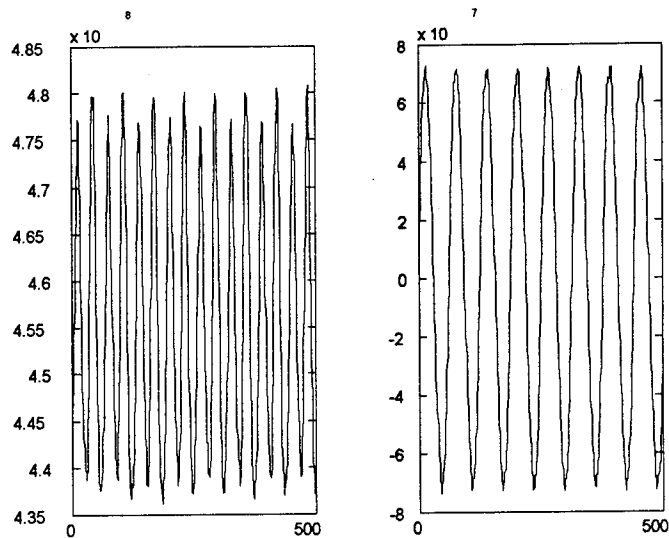


Figure 3.14 Denominator (Left plot) and Numerator (Right plot) Calculated Using Program TST7.ASM for Input Interferometric Signals of π Radians Optical Phase Shift at Frequency 0.0161fs.

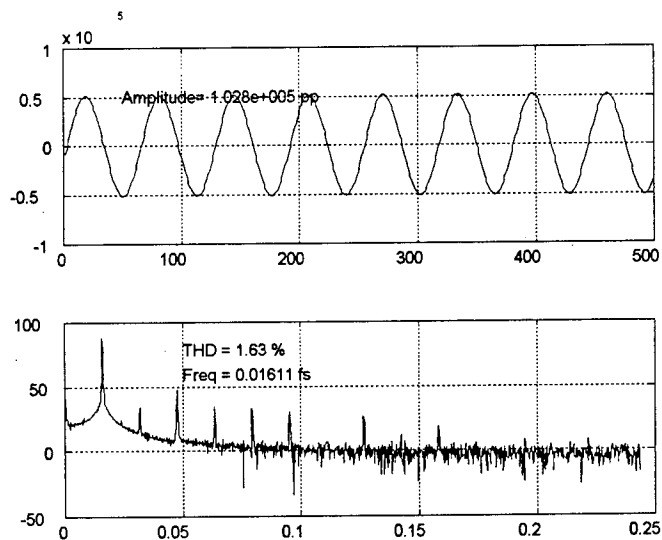


Figure 3.15 Demodulator Output for Interferometric Input of π Radians Optical Phase Shift at Frequency 0.0161fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

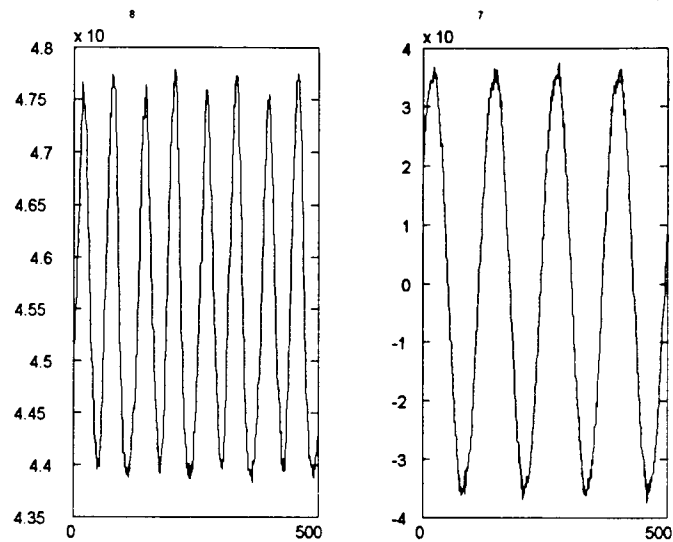


Figure 3.16 Denominator (Left plot) and Numerator (Right plot) Calculated Using Program TST7.ASM for Input Interferometric Signals of π Radians Optical Phase Shift at Frequency 0.0081fs.

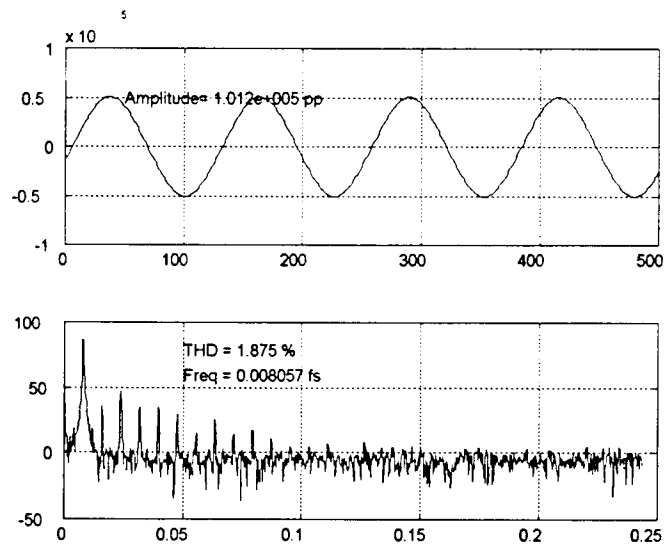


Figure 3.17 Demodulator Output for Interferometric Input of π Radians Optical Phase Shift at Frequency 0.0081fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

2. Demodulator Response to Optical Phase Shift Variations.

The demodulator response to variation in optical phase shifts was tested by simulating interferometric signals at a constant frequency of 600 Hz. The optical phase shift produced by the interferometric simulators was adjusted by setting the amplitude of the function generator driving the simulators to three different voltages, 0.01, 0.1 and 0.5 Volts peak. Using the scale factor for the simulators, this was equivalent to 9.33, 93.3, and 466.5 mrad of optical phase shift respectfully. In each run, 8192 points of the denominator, numerator and output signals were calculated by the demodulation programs and later downloaded to the PC. Plotting and analysis of the data was conducted in MATLAB using script files LDTST5.M and LDTST7.M. LDTST7.M is included in Appendix C. Power spectrum estimates were plotted using MATLAB's PSD.M script file from the signal processing toolbox, version. 3.1. The data was windowed using a 4096 point Hanning window thereby producing an equivalent noise bandwidth of 22.75 Hz. The power spectral density plots are plotted in dB's versus the Nyquist frequency. Figures 3.18 through 3.23, show demodulator output taken using the program TST5.ASM. Figures 3.24 through 3.29 show output taken using the program TST7.ASM. The estimates of the harmonic distortion were made using the fundamental and first ten harmonics.

From the plots, it would appear that both demodulation programs can demodulate reasonable ranges of interferometer optical phase shifts. However, demodulation program TST7.ASM, which uses floating point operations appears to have lower denominator fluctuations yet a higher distortion level in the output. Also, demodulation program TST7.ASM executes slightly faster than demodulation program TST5.ASM. Both programs have limited optical phase shift sensitivity because of the non constant denominator signal which is a result of non-simultaneous sampling. I was unable to test the demodulation programs in the multifringe range because of the limitation of the interferometric signal simulators. They could only produce a maximum optical phase shift of 2 pi radians.

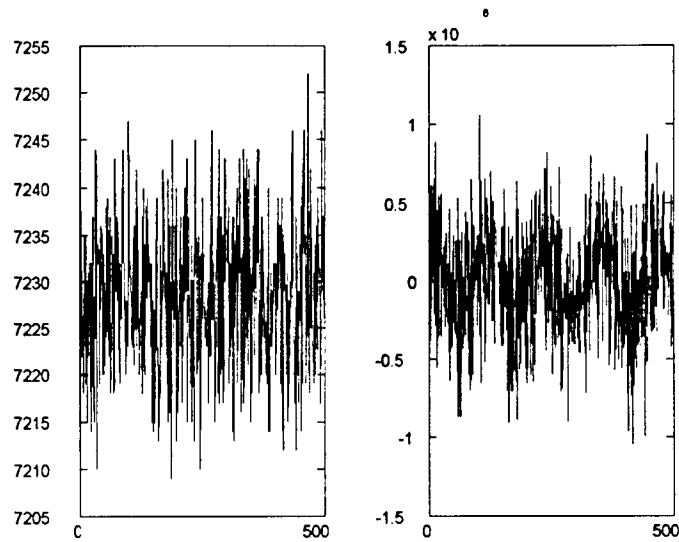


Figure 3.18 Denominator Divided by 2^{16} (Left plot) and Numerator (Right plot) Calculated using Program TST5.ASM for Input Interferometric Signals at 9.3 mrad Optical Phase Shift at Frequency 0.00864fs.

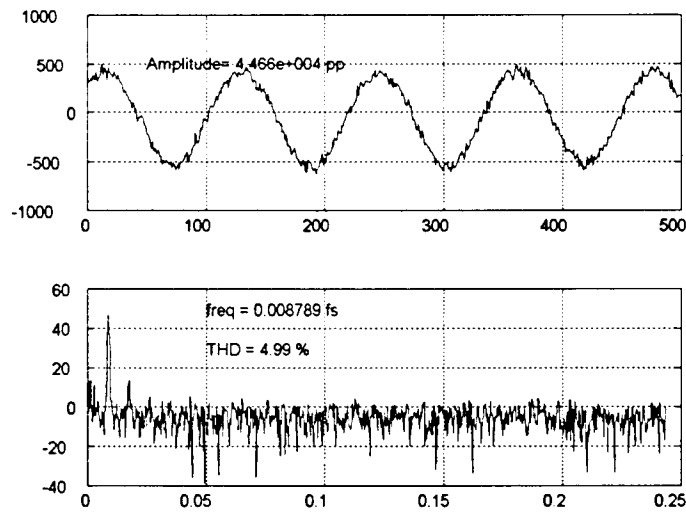


Figure 3.19 Demodulator Output Calculated using Program TST5.ASM for Input Interferometric Signals of 9.3 mrad of Optical Phase Shift at Frequency 0.00864fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

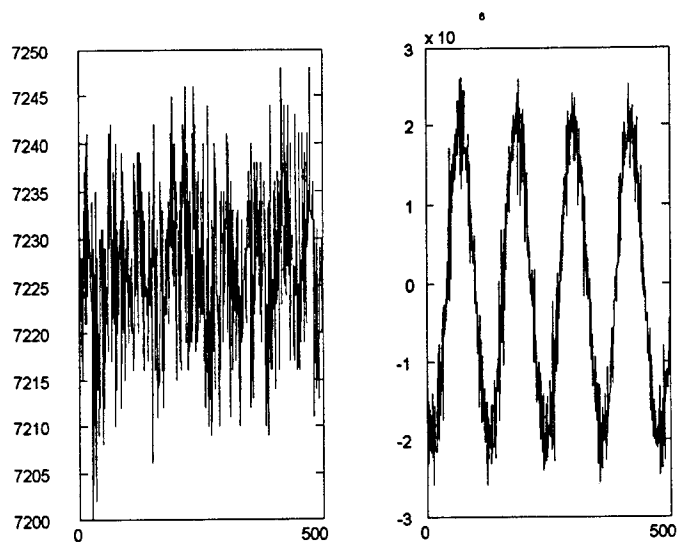


Figure 3.20 Denominator Divided by 2^{16} (Left plot) and Numerator (Right plot) Calculated using Program TST5.ASM for Input Interferometric Signals at 93.3 mrad Optical Phase Shift at Frequency 0.00864fs.

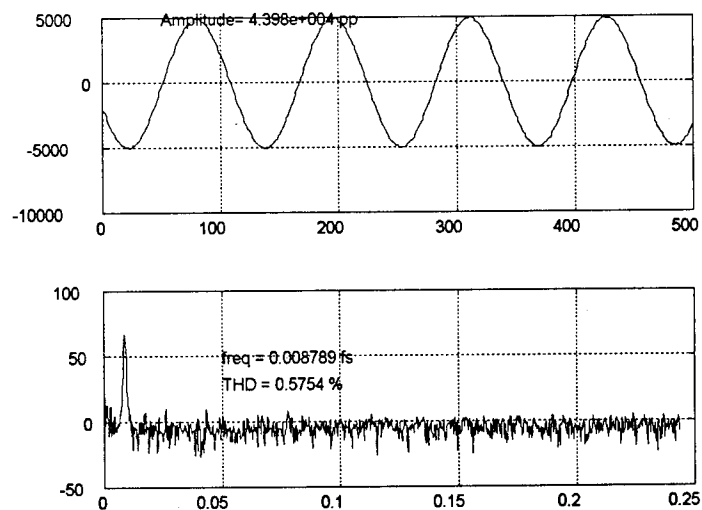


Figure 3.21 Demodulator Output Calculated using Program TST5.ASM for Input Interferometric Signals of 93.3 mrad of Optical Phase Shift at Frequency 0.00864fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

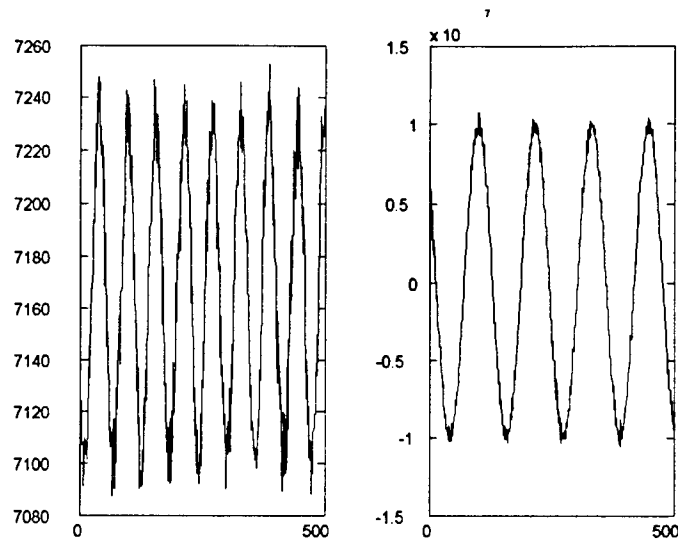


Figure 3.22 Denominator Divided by 2^{16} (Left plot) and Numerator (Right plot) Calculated using Program TST5.ASM for Input Interferometric Signals at 466.5 mrad Optical Phase Shift at Frequency 0.00864fs.

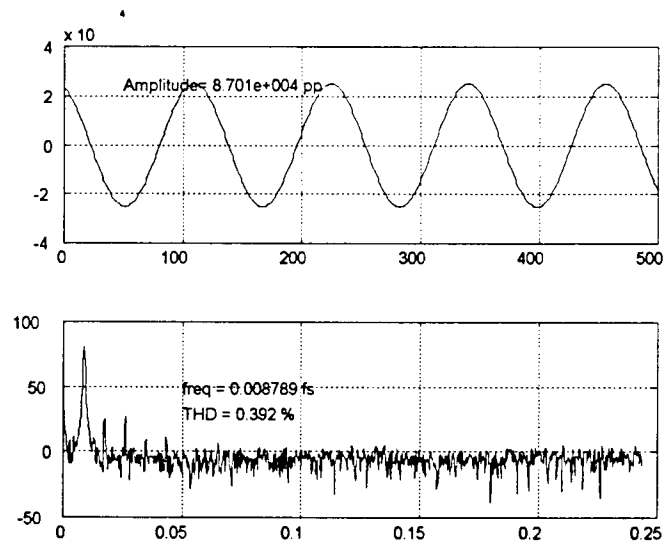


Figure 3.23 Demodulator Output Calculated using Program TST5.ASM for Input Interferometric Signals of 466.5 mrad of Optical Phase Shift at Frequency 0.00864fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

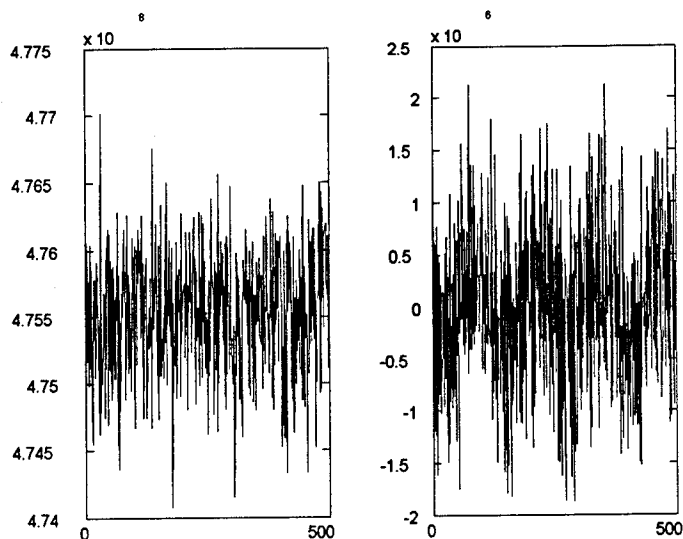


Figure 3.24 Denominator (Left plot) and Numerator (Right plot) Calculated using Program TST7.ASM for Input Interferometric Signals at 9.33 mrad Optical Phase Shift at Frequency 0.00792fs.

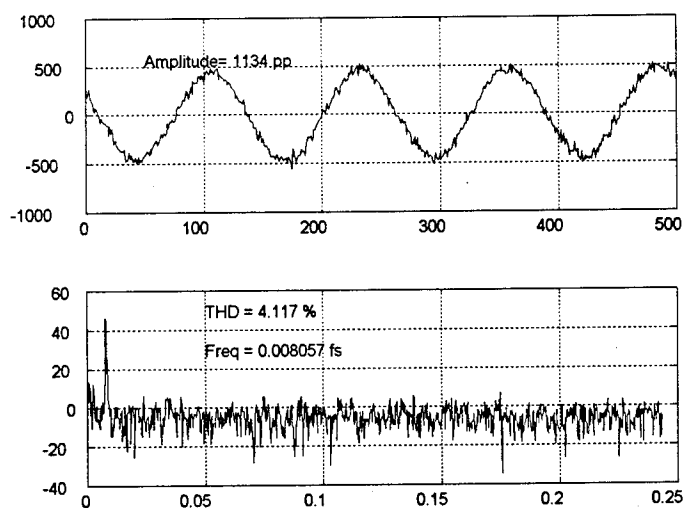


Figure 3.25 Demodulator Output Calculated using Program TST7.ASM for Input Interferometric Signals of 9.33 mrad of Optical Phase Shift at Frequency 0.00792fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

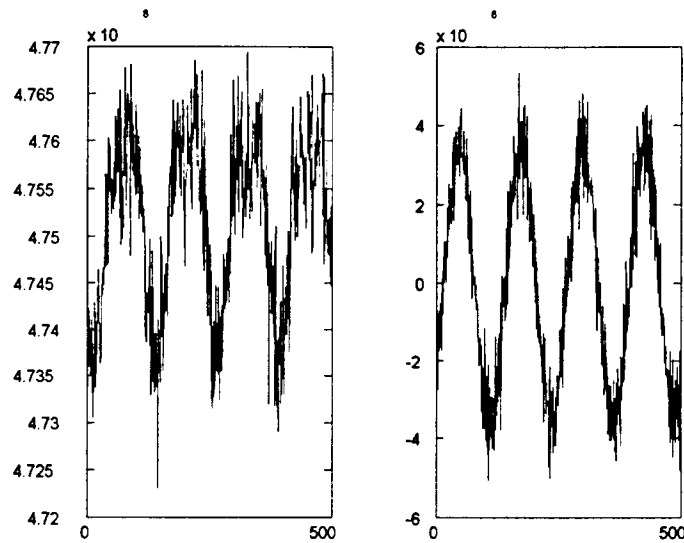


Figure 3.26 Denominator (Left plot) and Numerator (Right plot) Calculated using Program TST7.ASM for Input Interferometric Signals at 93.3 mrad Optical Phase Shift at Frequency 0.00792fs.

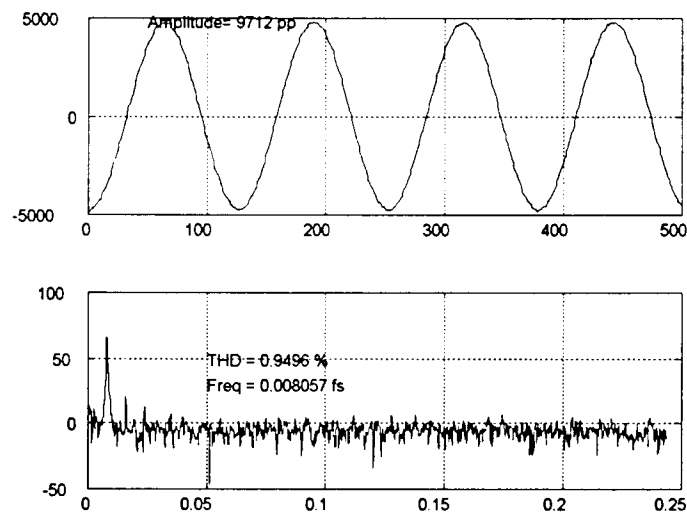


Figure 3.27 Demodulator Output Calculated using Program TST7.ASM for Input Interferometric Signals of 93.3 mrad of Optical Phase Shift at Frequency 0.00792fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

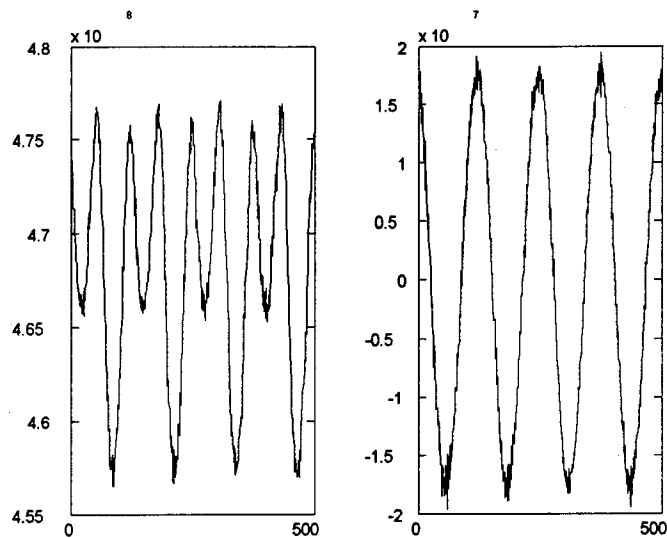


Figure 3.28 Denominator (Left plot) and Numerator (Right plot) Calculated using Program TST7.ASM for Input Interferometric Signals at 466.5 mrad Optical Phase Shift at Frequency 0.00792fs.

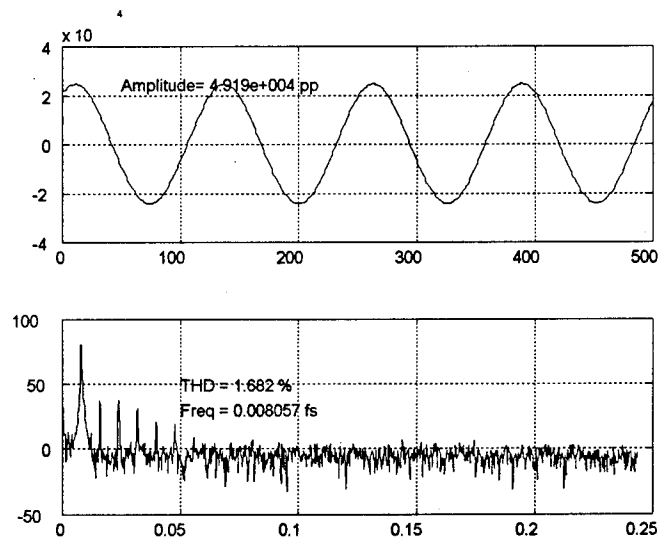


Figure 3.29 Demodulator Output Calculated using Program TST7.ASM for Input Interferometric Signals of 466.5 mrad of Optical Phase Shift at Frequency 0.00792fs. 500 Points of Demodulator Output (Upper plot). Power Spectrum of Output Plotted in dB's vs. Nyquist Frequency (Lower plot).

IV. DESIGN OF AN EXTERNAL SAMPLE AND HOLD CIRCUIT

This chapter discusses the design of an external sample and hold circuit which provided four channels of simultaneously sampled inputs. The PC31 limits analog input to two channels which can be sampled simultaneously using one DSP102. To obtain three analog input channels required the use of the internal multiplexing which resulted in non-simultaneous sampling. The results from the demodulation using non-simultaneous sampling clearly show an increase in output distortion caused by a non-stable denominator. Therefore, it was decided to build an external circuit which would provide simultaneous sampling.

A. DESIGN

The heart of the circuit involves three SHC5320 sample and hold IC's and an HI 507a multiplexer, refer to Figure 4.1, both from Burr-Brown [Ref 18]. The sample and hold IC's were configured in the non-inverting unity gain mode. They were supplied with ± 15 volts and the inputs were protected with input limiting diodes. Input to the three sample and holds can be from either the interferometric simulators or photo detected 3x3 coupler outputs. The outputs from the sample and hold are sent to input pair 1A and 1B, and input 2A of the multiplexer. Input 2B of the multiplexer is grounded. The outputs, OUT A and OUT B from the multiplexer are connected to inputs A and B of the DSP102.

The timing for the multiplexer and sample and hold circuitry is generated by the PC31 using internal timer #1, and the 82C54 timer, and by the external board using an 74HCT73, 74HCT109, and a 74HCT04. The timing of the sample and hold board is shown in Figure 4.2 for the designed sampling frequency of 100 kHz. The PC31's internal timer #1 (TCLK1) is configured to run as a square wave clock source with a frequency dependent upon the value loaded into the period register. A value of decimal 41 loaded into this register generated a clock frequency of 203.252 kHz. TCLK1 is used to generate the master timing clock. TCLK1 is routed from the PC31 to the external board where it is divided by two using one half of a 74HCT73 JK flip-flop, and one half of a 74HCT109 JK flip-flop. The 74HCT73 is rising edge triggered while the 109 is falling edge triggered. These two chips generate two timing clocks at one half the frequency of TCLK1, 101.626

kHz, one in phase with the rising edge of TCLK1, the other in phase with falling edge of TCLK1.

The rising edge of TCLK1 is used to gate timer/counter 0 of the 82C54. The 82C54 is a CMOS programmable interval timer. There is one such timer on the PC31 DSP board. The 82C54 has three independent 16 bit counters, which can operate in either BCD or binary counting. Each counter has six programmable modes of operation. Timer 0 is configured for mode 1, hardware retriggerable one-shot operation. When triggered by the rising edge of TCLK1, the output of timer 1, OUT0, goes low on the clock pulse following the trigger and remains low for the number of clock cycles loaded into the count register. The input clock source for counter 0 is the peripheral clock driver set to one quarter of the system clock, 8.33 MHz. Counter 0 is loaded with a count of decimal 9 which produces an output low signal of about 1.16 μ sec. OUT0 is then inverted by one 6th of a 74HCT04 and used as the convert signal for the DSP102.

Timer 1 of the 82C54 is also configured in mode 1, hardware retriggerable one-shot. The output from the 74HCT109, is used to trigger timer 1 on input GATE1 to the 82C54. OUT1 goes low on the clock pulse following the trigger and remains low for the number of clock cycles loaded in its count register. A value of decimal 58 loaded into the count register produces a low pulse of 7.2 μ sec on OUT1. This signal is also inverted by one sixth of a 74HCT04 and used to switch the Hold/Sample* input to the SHC5320's. The output from the 74HCT73 is used to drive pin A0 of the multiplexer. This pin when brought low selects input pair #1. A high on pin A0 selects input pair #2.

The SHC5320's are brought to the hold state within 200 nsec of the rising edge of TCLK1. Then the DSP102 is triggered by the falling edge of OUT0*, 1.16 μ sec after the rising edge of TCLK1. This gives the held output from the SHC5320's approximately 1 μ sec to settle before being sampled. At 2.5 μ sec after the rising edge of TCLK1 the falling edge of TCLK1 switches the multiplexer from input pair 1, (interferometric signals a and c), to input pair 2, (interferometric signal b and ground). This gives the multiplexer outputs approximately 3.6 μ sec in which to settle before being sampled, more than sufficient time to achieve 0.01% accuracy. 4.8 μ sec after the convert command to the DSP102, the first conversion is complete and interrupts the processor. The next conversion is signaled at 5.0 μ sec from the first, and after 1 μ sec the SHC5320's are brought to the sample state. This gives the sample and holds about 1.4 μ sec in which to re-track the input signal.

B. RESULTS OF CIRCUIT TESTING

With the external sample and hold circuit connected to the PC31, I was able to obtain four channels of analog input which could be simultaneously sampled at a maximum of 100 kHz. However, because the circuit was built on an external Proto-Board, with little consideration of interference, the noise levels at the input were greatly elevated, roughly on the order of 0.5 mV per channel. Nonetheless, I was able to implement the algorithm using this sampling circuit and the denominator signal was relatively constant, and the output showed signs of reduced distortion. A permanent board is currently being constructed by Professor Keolian for use with the PC31. This circuit was engineered to reduce the unwanted effects of external noise sources.

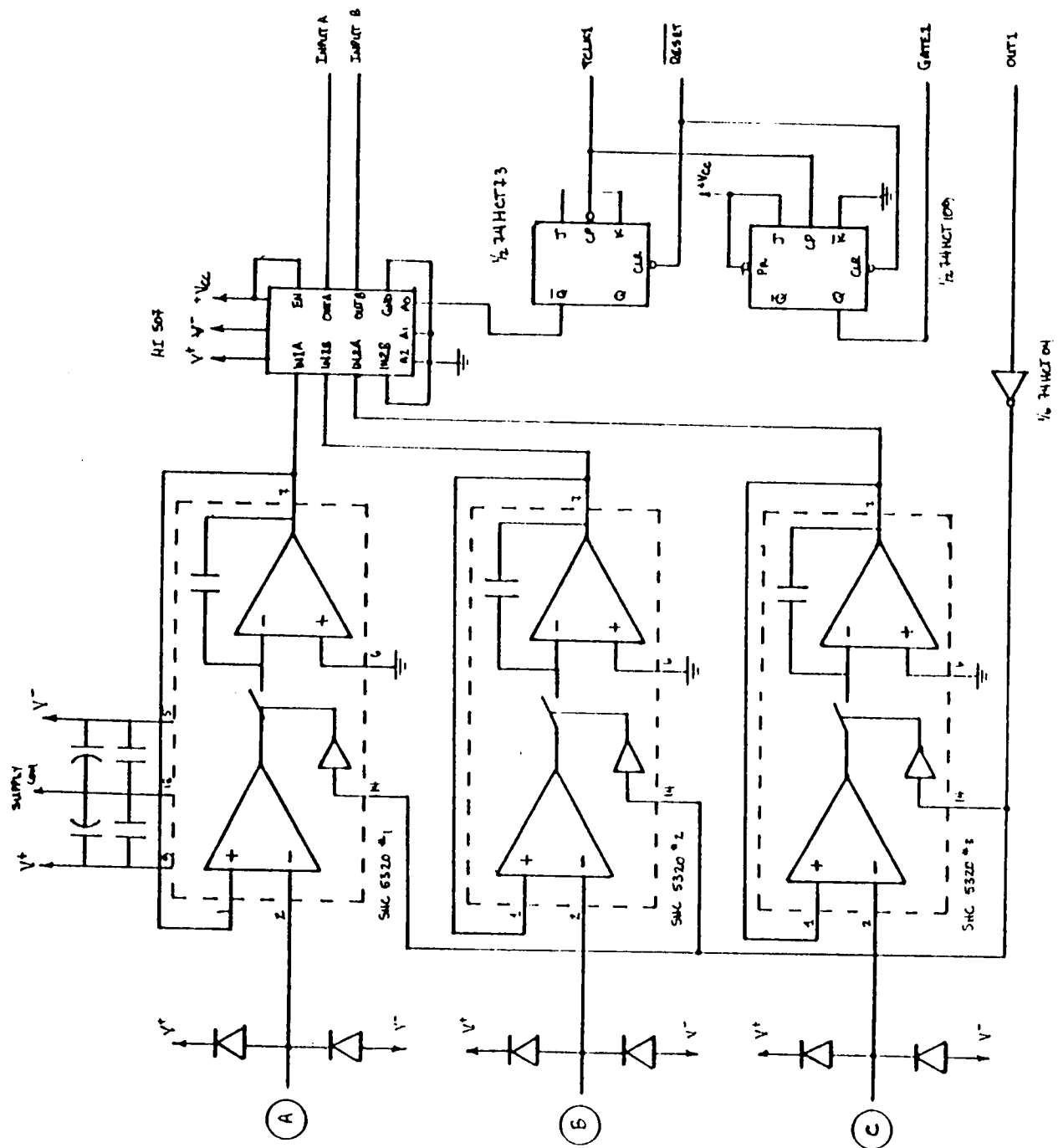


Figure 4.1 Schematic of external sample and hold circuitry.

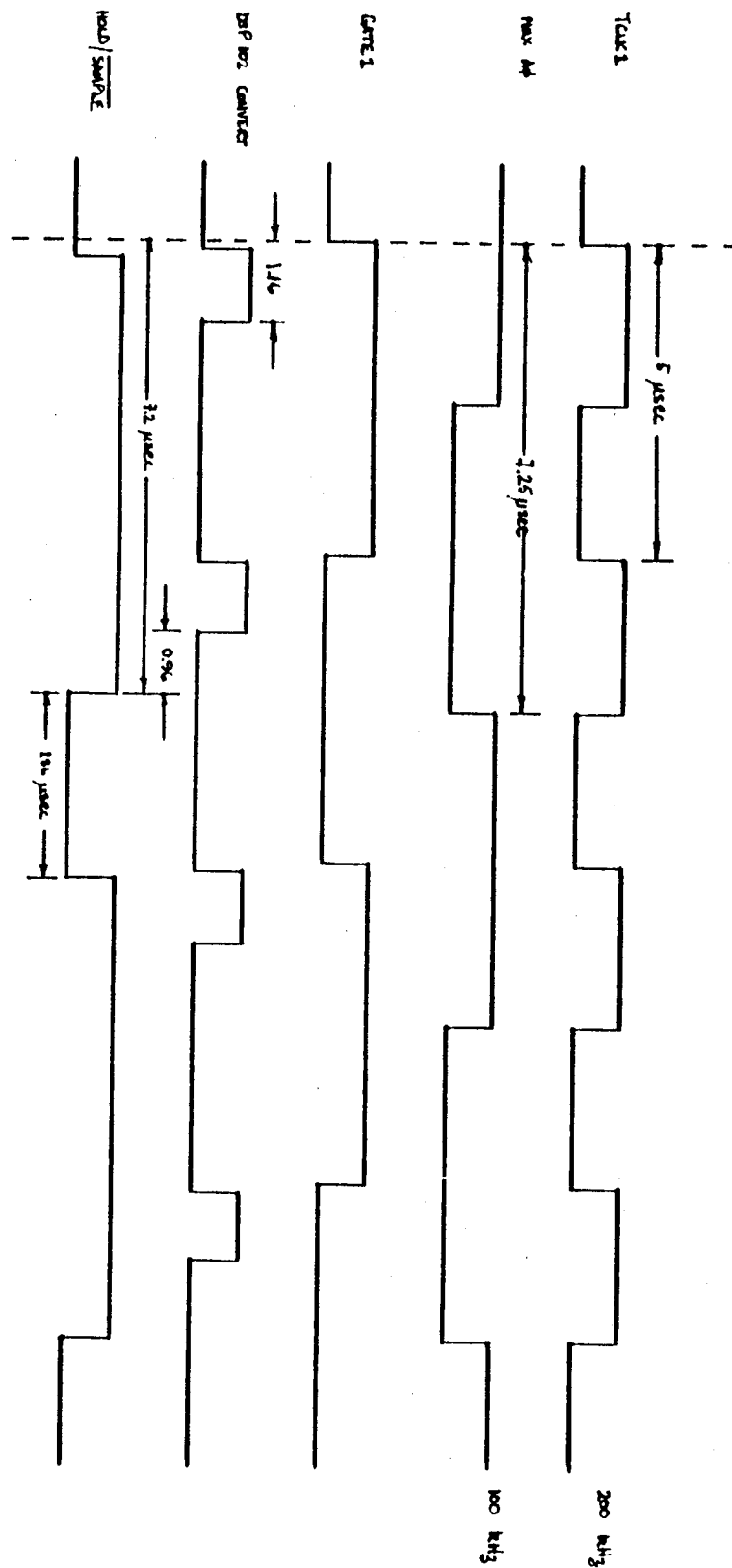


Figure 4.2 Timing diagram for external sample and hold circuit.

V. CONCLUSIONS AND RECOMMENDATIONS

This thesis has demonstrated that implementation of the symmetric demodulation scheme by digital signal processing hardware is possible and in fact extremely practical. It was shown that by using a DSP plug-in board, based upon the TMS320C31 DSP processor, the demodulation of three interferometric signals could execute in as little time as 10 μ sec. Using a first difference approach was suitable for calculation of the signal derivatives. The algorithm can be implemented using either fixed point integer or floating point operations, although the fixed point algorithm may take longer to execute. The demodulation execution time fixes the maximum sampling rate of the demodulator and thus the maximum allowable fringe rate, which is directly proportional to the sampling rate. The sensitivity of the demodulator is fixed by the size of the analog-to-digital quantization which is a function of the ADC. For a give sampling rate set by the demodulation process, increasing the conversion word size of the analog-to-digital converters will increase the sensitivity. Use of delta sigma converting ADCs, as suggested by McGinnis [Ref 9], was never considered, however, their usefulness could easily be verified in the future.

It was also shown that non-simultaneous sampling of the input interferometric signals leads to elevated levels of distortion in the output. These effects were not quantified and are left for follow-on research. An external sample and hold circuit was built and tested which would allow for the simultaneous sampling of up to four analog channels at a maximum of 100 kHz. This was shown to produce a fairly stable denominator signal which lead to reduced distortion in the output.

APPENDIX A. DSP CARD: PC31 BY INNOVATION INTEGRATION

The PC31 is a very high performance, IBM PC plug-in co-processor featuring the Texas Instruments TMS320C31 DSP processor. Lt. B. McGinnis had previously surveyed many DSP boards, and the PC31 was selected for its processing capabilities, analog section, good input-output support, and low cost. The TMS320C31 DSP processor meets all of the requirements for high-speed, real time applications: 17 MIPS/ 33 MFLOPS of processing power, hardware floating point multiplier/accumulator, DMA controller, on chip synchronous serial port ADC and DAC.

Software is interactively developed and tested using the optimizing ANSI compatible C compiler. Applications are developed and tested using the integer and floating point math, analog/digital I/O and video display libraries provided with the Developers package. All systems and application procedures may conveniently be interactively edited, tested and executed at full machine speed.

The Board serves as its own development system using the system monitor resident in the IBM PC host in combination with other essential software tools supplied with the Developers package. Once an application has been created, it may be embedded in PROM for stand alone operation or downloaded to the board from within the system monitor. The PC31 communicates with an IBM PC/AT, or equivalent, via a high speed dual port memory arrangement which allows access to all PC31 memory and peripherals from the IBM PC.

Interfacing with external peripherals is accomplished with two 10-pin serial ports, one 37-pin analog connector, one 50-pin digital connector or one 108 pin expansion connector. Additionally, the PC31 is compatible with the full line of DSP-LINK analog and digital I/O cards.

APPENDIX B. ANALOG INTERFEROMETRIC SIGNAL SIMULATOR

The analog interferometric signal simulator built by Dr. David Gardner, is similar to that described in [Ref 7:Appendix C]. Additional modifications were made to the circuit and are described in [Ref 19:pp 73-75]. The simulator was built around Analog Device's AD639 Universal Trigonometric Function Converter (refer to Figure B1). Adjustments on the simulator provide for the setting of the static phase angle and output signal amplitude, however, the drift angle term is not time-varying as it would be in an actual system. By configuring three simulators together and adjusting the static phase angle of each, three interferometric waveforms separated by 120° can be generated for any bias angle.

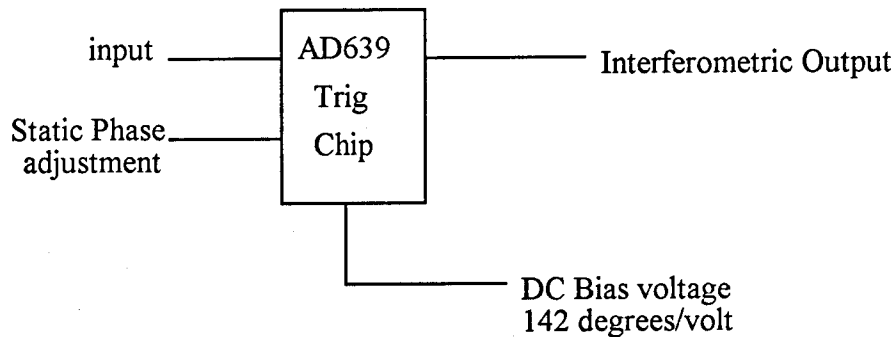


Figure B1 Block diagram of interferometric signal simulator taken from Ref 9

The Analog Devices AD639 Universal Trigonometric Function Converter is configured to produce the sine of its input. A one volt input is equivalent to an input argument of 50° . The gain of the circuit built by Gardner [Ref 7] was set to 2.85. Thus the static phase adjustment input equates to,

$$2.85 \times 50^\circ/\text{Volt} = 142^\circ/\text{Volt}, \quad (\text{B.1})$$

so that, with one simulator adjusted to zero volts static phase output and the other two static phase outputs adjusted to ± 0.845 V, three interferometric signals symmetrically phase shifted 120° relative to each other will be produced.

As designed, the simulators produced a maximum output of 3.6 V peak to peak. This was well within the range of allowed for input voltages to the DSP102. However, they are not able to produce the dc offset voltage which is associated with real interferometric signals. The simulators were able to generate outputs for input signal amplitudes of up to 8.0 Volts peak-to-peak ($\cong 2 \pi$ radians). Above 8.0 volts, the simulators become severely distorted due to saturation in the analog electronics. The average scale factor for the three interferometric simulators was reported to be 0.933 rad/Volt [Ref 9 p 51]. The average phase noise was reported to be $0.48 \pm 0.005 \mu\text{rad}/\sqrt{\text{Hz}}$ measured at 1 kHz in a one Hz bandwidth [Ref 19:p 64].

APPENDIX C. MISCELLANEOUS

This appendix contains the following:

1. Turbo C programs written for this thesis.

TCDEMOD.C

2. MATLAB script files written for this thesis.

PLOTDAT.M

DEMOD.M

PLOTABC.M

LDTST3.M

LDTST7.M

3. PC31 C programs written for this thesis.

TMSDEMOD.C

4. PC31 Assembly language programs written for this thesis.

TST3.ASM

TST5.ASM

TST7.ASM

A. PROGRAM TCDEMOC.C

```
/******
*
*   TCDEMOC.C - Test routine written in Turbo C.
*   This program generates the three channels output from a 3x3
*   fiber optic interferometer. The 3 channels are then
*   demodulated using a symmetric demodulation scheme using
*   integer arithmetic. The output is accumulated in the variable
*   phase
*
*   Written by : LCdr Brenner 09 Feb 1994
*
*   last modified : 11 Aug 94
*
*****/

#include "stdio.h"
#include "math.h"
#define num_samples 1024
#define onethird 1.0/3.0
#define decay 0.999

void main(void);
void gen_signal(void);

void main()
{
    extern int A[num_samples];
    extern int B[num_samples];
    extern int C[num_samples];
    long int output[num_samples];
    long int denom[num_samples];
    long int numer[num_samples];
    long int a[num_samples];
    long int b[num_samples];
    long int c[num_samples];
    long int adot[num_samples];
    long int bdot[num_samples];
    long int cdot[num_samples];
    long int a_temp, b_temp, c_temp, numer1, numer2, numer3;
    int i, offset;
    FILE *fp;

    a_temp = 0; b_temp = 0; c_temp = 0;
    numer1 = 0; numer2 = 0; numer3 = 0;
    offset = 0;

    fp = fopen("demod.dat", "w+b");
```



```

gen_signal();

for(i = 0; i < num_samples; i++)
{
    offset = (int)(onethird*(A[i] + B[i] + C[i]));
    a[i] = (A[i] - offset);
    b[i] = (B[i] - offset);
    c[i] = (C[i] - offset);

    denom[i] = (a[i]*a[i] + b[i]*b[i] + c[i]*c[i]) >> 16;
    adot[i] = a[i] - a_temp;
    bdot[i] = b[i] - b_temp;
    cdot[i] = c[i] - c_temp;
    numer1 = a[i]*(cdot[i] - bdot[i]);
    numer2 = b[i]*(adot[i] - cdot[i]);
    numer3 = c[i]*(bdot[i] - adot[i]);
    numer[i] = numer1 + numer2 + numer3;

    output[i] = (long int)(decay*output[i-1]) + numer[i]/denom[i];

    a_temp = a[i]; b_temp = b[i]; c_temp = c[i];
}
fwrite(a, sizeof(long int), num_samples, fp);
fwrite(adot, sizeof(long int), num_samples, fp);
fwrite(b, sizeof(long int), num_samples, fp);
fwrite(bdot, sizeof(long int), num_samples, fp);
fwrite(c, sizeof(long int), num_samples, fp);
fwrite(cdot, sizeof(long int), num_samples, fp);
fwrite(denom, sizeof(long int), num_samples, fp);
fwrite(numer, sizeof(long int), num_samples, fp);
fwrite(output, sizeof(long int), num_samples, fp);
fclose(fp);
}

/*
 *
 * Routine to generate interferometric waveforms
 *
 */
int A[num_samples];
int B[num_samples];
int C[num_samples];

void gen_signal()
{
    int i, scale;
    float Ac, f, fs, Light_amp, pi;
    float theta[num_samples];

    pi = 4.0*atan(1.0);
    fs = 1.0/128.0;

```

```

Ac = pi;
Light_amp = 0.0;
scale = 32000;

for(i = 0; i < num_samples; i++)
{
    theta[i] = 2.0*pi*fs*i;
    A[i] = (Light_amp + cos(Ac*sin(theta[i]) - pi/6))*scale;
    B[i] = (Light_amp + cos(Ac*sin(theta[i]) + pi/2))*scale;
    C[i] = (Light_amp + cos(Ac*sin(theta[i]) + 7*pi/6))*scale;
}
}

```

B. PROGRAM PLOTDAT.M

```
%*****
%
% PLOTDAT.M - Plots data generated by the C program DEMOD1.C
%
% Written by: LCdr Brenner  10 Aug 94
%
%*****

clear all, clc, clf

N = 2048;

A = ld16bit('c:\tc\thesis\demod1.dat',N,0);
B = ld16bit('c:\tc\thesis\demod1.dat',N,N);
C = ld16bit('c:\tc\thesis\demod1.dat',N,2*N);
output = ld32bit('c:\tc\thesis\demod1.dat',N,3*N/2);

L = 200;
l = 0:L-1;
figure(1)
plot(l,A(1:L),':',l,B(1:L),'--',l,C(1:L))

figure(2)
subplot(211),plot([0:1999],output(1:2000))
disp(['Max output = ',num2str(max(output)), ' Min output = ',num2str(min(output))])

Nfft = N; fs = 100e3;
w = hanning(Nfft);
[Pxx,fx] = psd(output,Nfft,fs,w,256);
Pxx = Pxx*norm(w)^2/sum(w)^2;
subplot(212),plot(fx/fs,10*log10(Pxx)),grid
%[x,y] = ginput(6);
%y = 10.^(y/20);
%THD = sum(y(2:6))/y(1)*100;
%text(10e3,110,['THD = ',num2str(THD),' %'])
```

C. PROGRAM DEMOD.M

```
%*****
%
% DEMOD.M - this program plots theoretical interferometric signals
%      for a three leg interferometer. And then demodulates them using
%      a symetric demodulation technique.
%
%      written by: LCdr Brenner  7 June 94
%      Last modified : 20 July 94
%
%*****

clear all,clf,clc

N = 1024;
%diary demod1.txt

%set acoustic amplitude plus noise.
noise = 0;
phase_shift = pi;
Ac = phase_shift*ones(1,N) + noise*randn(1,N);
disp(['optical phase shift = ',num2str(phase_shift),' radians'])

%set sampling frequency f/fs
fs = 100e3; f = 600;
disp(['sampling freq = ',num2str(fs),' Hz'])
disp(['acoustic frequency = ',num2str(f),' Hz'])

%calculate sampled phase angle
theta = (2*pi*f/fs)*[1:N];

%set phase noise term (static phase difference plus drift)
phid_noise = 0.0;
phid = phid_noise*rand(1,N);

%calculate input signal
signal = Ac.*sin(theta + phid);

%set laser amplitude and measurement noise
Dc = 0.5/2.75;
samp = 5.0;
sampling_noise = samp.*randn(1,N);

%generate theoretical interferometric signals
scale = 2^15;
A = fix((Dc + cos(signal - pi/6))*scale) + sampling_noise;
B = fix((Dc + cos(signal + pi/2))*scale) + sampling_noise;
C = fix((Dc + cos(signal + 7*pi/6))*scale) + sampling_noise;
```

```

% initialize variables
decay = 0.99;
offset1 = fix(1/3*(A(1) + B(1) + C(1)));
offset2 = fix(1/3*(A(2) + B(2) + C(2)));
a1 = fix(A(1) - offset1); a2 = fix(A(2) - offset2);
b1 = fix(B(1) - offset1); b2 = fix(B(2) - offset2);
c1 = fix(C(1) - offset1); c2 = fix(C(2) - offset2);
denom = fix((a1^2 + b1^2 + c1^2)/2^16);
adot = fix(a2 - a1); atemp = a1;
bdot = fix(b2 - b1); btemp = b1;
cdot = fix(c2 - c1); ctemp = c1;
numer = fix(a1*(cdot - bdot) + b1*(adot - cdot) + c1*(bdot - adot));
last_output = numer/denom;

%run algorithm
for k = 1:N
    offset = fix(1/3*(A(k) + B(k) + C(k)));
    a = A(k) - offset;
    b = B(k) - offset;          %subtract dc from interferometric signals
    c = C(k) - offset;
    denom(k) = fix((a^2 + b^2 + c^2)/2^16);    %calculate factor that accounts for laser power
    adot(k) = a - atemp;
    bdot(k) = b - btemp;        %calcluate derivatives of signals
    cdot(k) = c - ctemp;
    numer1(k) = fix(a*(cdot(k) - bdot(k)));
    numer2(k) = fix(b*(adot(k) - cdot(k)));
    numer3(k) = fix(c*(bdot(k) - adot(k)));
    numer(k) = fix(numer1(k) + numer2(k) + numer3(k));
    output(k) = fix(decay*last_output + numer(k)/denom(k));

    atemp = a; btemp = b; ctemp = c; last_output = output(k);
end

figure(1)
L = 200; l = 0:L-1;
subplot(131),plot(l,A(1:L))
subplot(132),plot(l,B(1:L))
subplot(133),plot(l,C(1:L))
disp(['max A = ',num2str(max(A)), ' min A = ',num2str(min(A))])
disp(['max B = ',num2str(max(B)), ' min B = ',num2str(min(B))])
disp(['max C = ',num2str(max(C)), ' min C = ',num2str(min(C))])

figure(2)

subplot(311),plot(adot)
disp(['max adot = ',num2str(max(adot)), ' min adot = ',num2str(min(adot))])
subplot(312),plot(bdot)
disp(['max bdot = ',num2str(max(bdot)), ' min bdot = ',num2str(min(bdot))])
subplot(313),plot(cdot)
disp(['max cdot = ',num2str(max(cdot)), ' min cdot = ',num2str(min(cdot))])

```

figure(3)

```
subplot(311),plot(number1)
disp(['max number1 = ',num2str(max(number1)), ' min number1 = ',num2str(min(number1))])
subplot(312),plot(number2)
disp(['max number2 = ',num2str(max(number2)), ' min number2 = ',num2str(min(number2))])
subplot(313),plot(number3)
disp(['max number3 = ',num2str(max(number3)), ' min number3 = ',num2str(min(number3))])
```

figure(4)

```
subplot(211),plot(number(1:300))
disp(['max number = ',num2str(max(number)), ' min number = ',num2str(min(number))])
subplot(212),plot(denom(1:300))
disp(['max denom = ',num2str(max(denom)), ' min denom = ',num2str(min(denom))])
```

figure(5)

```
subplot(211),plot(output(1:1000))
```

```
Nfft = 1024;
w = hanning(Nfft);
[Pxx,fx] = psd(output,Nfft,fs,w,256);
Pxx = Pxx*norm(w)^2/sum(w)^2;
subplot(212),plot(fx/fs,10*log10(Pxx)),grid
[x,y] = ginput(11);
y = 10.^(y/20);
THD = sum(y(2:11))/y(1)*100;
text(0.1,100,['THD = ',num2str(THD),' %'])
```

```
disp('-----')
diary off
```

D. PROGRAM PLOTABC.M

```
%*****
%
% PLOTABC.M - Plots test data taken from the PC31.
%   This script file assumes that data has been
%   taken from the PC31 using TST3.ASM
%
%   Written by LCdr Brenner 10 Aug 94
%
%*****

clear all, clf, clc
Nfft = 4096;
fs = 75757.6;
w = hanning(Nfft);
%a0 = 0.35875; a1 = 0.48829; a2 = 0.14128; a3 = 0.01168; n = 0:Nfft-1;
%w = a0 - a1*cos(2*pi*n/Nfft) + a2*cos(4*pi*n/Nfft) - a3*cos(6*pi*n/Nfft);

a_gnd = ld16bit('a_gnd.dat');
b_gnd = ld16bit('b_gnd.dat');
c_gnd = ld16bit('c_gnd.dat');

afull = ld16bit('amux600.dat');
bfull = ld16bit('bmux600.dat');
cfull = ld16bit('cmux600.dat');
figure(1)
subplot(211),plot(afull(1:1000))
%title(['Data A multiplexed on channel a (sampling freq = ',num2str(fs),' Hz)'])
text(100,3.5e4,['Max = ',num2str(max(afull)),',Min = ',num2str(min(afull))])
[Paa,fa] = psd(afull(1:Nfft),Nfft,fs,w,256);
Paa = Paa*norm(w)^2/sum(w)^2;
subplot(212),plot(fa(1:1000)/fs,10*log10(Paa(1:1000)))
%ylabel('Magnitude - dB')
SNR = 10*log10(max(Paa)/mean(Paa(1000:Nfft/2)));
text(0.025,80,['SNR = ',num2str(SNR),' dB'])
[x,y] = ginput(11);
y = 10.^(y/20);
THD = sum(y(2:11))/y(1)*100;
text(0.025,50,['THD = ',num2str(THD),' %'])
figure(2)
subplot(211),plot(bfull(1:1000))
%title(['Data B multiplexed on channel a (sampling freq = ',num2str(fs),' Hz)'])
text(100,3.5e4,['Max = ',num2str(max(bfull)),',Min = ',num2str(min(bfull))])
[Pbb,fb] = psd(bfull(1:Nfft),Nfft,fs,w,256);
Pbb = Pbb*norm(w)^2/sum(w)^2;
subplot(212),plot(fb(1:1000)/fs,10*log10(Pbb(1:1000)))
%ylabel('Magnitude - dB')
SNR = 10*log10(max(Paa)/mean(Paa(1000:Nfft/2)));
text(0.025,80,['SNR = ',num2str(SNR),' dB'])
```

```

[x,y] = ginput(11);
y = 10.^(y/20);
THD = sum(y(2:11))/y(1)*100;
text(0.025,50,['THD = ',num2str(THD),' %'])
figure(3)
subplot(211),plot(cfull(1:1000))
%title(['Data C on channel b (sampling freq = ',num2str(fs),' Hz)'])
text(100,3.5e4,['Max = ',num2str(max(cfull)),',Min = ',num2str(min(cfull))])
[Pcc,fc] = psd(cfull(1:Nfft),Nfft,fs,w,256);
Pcc = Pcc*norm(w)^2/sum(w)^2;
subplot(212),plot(fc(1:1000)/fs,10*log10(Pcc(1:1000)))
%ylabel('Magnitude - dB')
SNR = 10*log10(max(Paa)/mean(Paa(1000:Nfft/2)));
text(0.025,80,['SNR = ',num2str(SNR),' dB'])
[x,y] = ginput(11);
y = 10.^(y/20);
THD = sum(y(2:11))/y(1)*100;
text(0.025,50,['THD = ',num2str(THD),' %'])
figure(4)
subplot(211),plot(a_gnd(1:500))
%title(['Data A multiplexed on channel a (sampling freq = ',num2str(fs),' Hz)'])
text(50,15,['Max = ',num2str(max(a_gnd)),', Min = ',num2str(min(a_gnd))])
text(50,-15,['Mean = ',num2str(mean(a_gnd))])
[Paa,fa] = psd(a_gnd(1:Nfft),Nfft,fs,w,256);
Paa = Paa*norm(w)^2/sum(w)^2;
subplot(212),plot(fa/fs,10*log10(Paa))
%ylabel('Magnitude - dB')
text(5e3,-10,['Mean = ',num2str(10*log10(mean(Paa))),', dB'])
figure(5)
subplot(211),plot(b_gnd(1:500))
%title(['Data B multiplexed on channel a (sampling freq = ',num2str(fs),' Hz)'])
text(50,15,['Max = ',num2str(max(b_gnd)),', Min = ',num2str(min(b_gnd))])
text(50,-15,['Mean = ',num2str(mean(b_gnd))])
[Pbb,fb] = psd(b_gnd(1:Nfft),Nfft,fs,w,256);
Pbb = Pbb*norm(w)^2/sum(w)^2;
subplot(212),plot(fb/fs,10*log10(Pbb)),axis([0 0.5 -60 0])
%ylabel('Magnitude - dB')
text(5e3,-10,['Mean = ',num2str(10*log10(mean(Pbb))),', dB'])
figure(6)
subplot(211),plot(c_gnd(1:500))
%title(['Data C on channel b (sampling freq = ',num2str(fs),' Hz)'])
text(50,15,['Max = ',num2str(max(c_gnd)),', Min = ',num2str(min(c_gnd))])
text(50,-15,['Mean = ',num2str(mean(b_gnd))])
[Pcc,fc] = psd(c_gnd(1:Nfft),Nfft,fs,w,256);
Pcc = Pcc*norm(w)^2/sum(w)^2;
subplot(212),plot(fc/fs,10*log10(Pcc))
%ylabel('Magnitude - dB')
text(5e3,-10,['Mean = ',num2str(10*log10(mean(Pcc))),', dB'])

```


E. PROGRAM LDTST3.M

```
%*****
%
% LDTST3.M loads data from taken from PC31 digital demodulator
%      using TST3.asm program.
%      Amux, Bmux and Cmux data are loaded and plotted.
%
%      written by; LCdr Brenner 29 Aug 94
%
%*****
clear all, clf
Nfft = 4096;
fs = 75757.6;
w = hanning(Nfft);
%a0 = 0.35875; a1 = 0.48829; a2 = 0.14128; a3 = 0.01168; n = 0:Nfft-1;
%w = a0 - a1*cos(2*pi*n/Nfft) + a2*cos(4*pi*n/Nfft) - a3*cos(6*pi*n/Nfft);

num = input('Input data number to be loaded ','s');
filename1 = ['b:amux',num,'.dat'];
amux = ld16bit(filename1);
filename2 = ['b:bmux',num,'.dat'];
bmux = ld16bit(filename2);
filename3 = ['b:cmux',num,'.dat'];
cmux = ld16bit(filename3);
%plot the data
figure(1)
subplot(211),plot(amux(2:1000))
[Paa,fa] = psd(amux(2:Nfft),Nfft,fs,w,256);
Paa = Paa*norm(w)^2/sum(w)^2;
subplot(212),plot(fa(1:1000)/fs,10*log10(Paa(1:1000)))
SNR = 10*log10(max(Paa)/mean(Paa(100:Nfft/2)));
text(0.025,30,['SNR = ',num2str(SNR),' dB'])
figure(2)
subplot(211),plot(bmux(2:1000))
[Pbb,fb] = psd(bmux(2:Nfft),Nfft,fs,w,256);
Pbb = Pbb*norm(w)^2/sum(w)^2;
subplot(212),plot(fb(1:1000)/fs,10*log10(Pbb(1:1000))),axis([0 0.25 -50 50])
SNR = 10*log10(max(Pbb)/mean(Pbb(100:Nfft/2)));
text(0.025,30,['SNR = ',num2str(SNR),' dB'])
figure(3)
subplot(211),plot(cmux(2:1000))
[Pcc,fc] = psd(cmux(2:Nfft),Nfft,fs,w,256);
Pcc = Pcc*norm(w)^2/sum(w)^2;
subplot(212),plot(fc(1:1000)/fs,10*log10(Pcc(1:1000)))
SNR = 10*log10(max(Pcc)/mean(Pcc(100:Nfft/2)));
text(0.025,30,['SNR = ',num2str(SNR),' dB'])
```

F. PROGRAM LDTST7.M

```
%*****
%
% LDTST7.M loads data taken from PC31 digital demodulator
%   using TST7.ASM program. TST7 demodulates the signals
%   using floating point math. Denominator, numerator and
%   output samples are stored. 4096 points of data are loaded
%   by this program.
%
%   written by; LCdr Brenner 29 Aug 94
%
%*****

clear all, clf, clc

num = input('Input data number to be loaded ','s');
filename1 = ['denf',num,'.dat'];
denom = ld32bit(filename1);
filename2 = ['numf',num,'.dat'];
numer = ld32bit(filename2);
filename3 = ['outf',num,'.dat'];
output = ld32bit(filename3);
N = length(output); fs = 75757.6;

%plot the data

figure(1)
L = 500; l = 0:L-1;
subplot(121),plot(l,denom(L:2*L-1))
amp = max(denom)-min(denom);
disp(['Swing= ',num2str(amp)])
subplot(122),plot(l,numer(L:2*L-1))
amp = max(numer)-min(numer);
disp(['Swing= ',num2str(amp)])

figure(2)
subplot(211),plot(output(N-L+1:N)),grid
text(50,max(output),['Amplitude= ',num2str(max(output)-min(output)),' pp'])

Nfft = 4096;
w = hanning(Nfft);
[Pxx,fx] = psd(output(N-Nfft:N),Nfft,fs,w,256);
Pxx = Pxx*norm(w)^2/sum(w)^2;
subplot(212),plot(fx(1:1000)/fs,10*log10(Pxx(1:1000))),grid
text(0.05,60,['Freq = ',num2str(find(Pxx == max(Pxx))/Nfft),' fs'])
[x,y] = ginput(6);
y = 10.^(y/20);
THD = sum(y(2:6))/y(1)*100;
```

```
text(0.05,80,['THD = ',num2str(THD),' %'])
```

G. PROGRAM TMSDEMOC.C

```
/******
*
*      TMSdemoc.c - 4
*      This program was written for compilation using the TMS320 optimizing C compiler.
*      Data presented on MUX channels IN0 and IN1 and inputB of the DSP102 are sampled
*      and then asymmetric demodulation is performed using integer arithmetic.
*      4000 points of output data are accumulated in the vectors phase and denom.
*
*      written by LCdr Brenner 10 Mar 1994.
*      last modified : 01 May 94
*
*****/

#include "stdio.h"                      /* constant definitions for PC31 */
#define num_samples 4000                /* number of data samples to take */
#define DECAY 0.99                      /* set integrator decay constant */

int main(void);
int denom[num_samples];                 /* denominator term */
int output[num_samples];                /* output of algorithm */

main()
{
    volatile int* ser_gc = SER_GC;
    volatile int* adc = ADC;
    volatile int* da0 = DAC0;
    volatile int* da1 = DAC1;
    volatile int* ser_rd = SER_RD;
    volatile int* ser_td = SER_TD;
    int i, a, b, c, a_temp, b_temp, c_temp;
    int adot, bdot, cdot, numer, square, start, stop;
    a_temp = 0; b_temp = 0; c_temp = 0;
    denom[0] = 0;
    output[0] = 0;

    set_ST(get_ST() | 0x0800);           /* Enable PC31 cache */
    enable_interrupts();
    timer(2,1000);                       /* set up 1Khz timebase on channel */
    enable_clock();                      /* 2 of 8254 timer */

    *ser_gc = 0x0ebd0040;                /* initialize serial communications */
    *SER_FSX = 0x00000111;               /* with DSP102,202, 32 bit words */
    *SER_FSR = 0x00000111;               /* chan A MSB, chan B LSB, polled */
    *SER_CTL = 0x0000000f;               /* operation */
    *SER_CNT = 0;
    *SER_PER = 0;

    *MUX_A = 0;                          /* Use Mux A channel IN0, IN1 */
}
```

```

*ser_td = 0;
*da0;
while((*ser_gc & 2) == 0)
;
/* set all DSP102 DACs to zero */
/* output voltage state */
*ser_td = 0;
*da1;
while((*ser_gc & 2) == 0)
;
*ser_rd;
/* dummy reads of serial input port */
*ser_rd;
/* to clear for first conversion */
*adc;
/* convert data on Mux channel IN0 */
*MUX_A = 1;
/* switch Mux to IN1 prior to next conv */
start = uclock();

for(i = 1; i <= num_samples; i++)
/* start of demodulation loop */
{
    while((*ser_gc & 1) == 0)
    /* wait till prev conv complete */
    ;
    *adc;
    /* start next conv (data b,Mux 1) */
    *MUX_A = 0;
    /* switch Mux back to IN0 for data A */
    a = *ser_rd >> 16;

    while((*ser_gc & 1) == 0)
    /* wait for conv( 4.8 usec) data b and c */
    /* being sampled */
    ;
    temp = *ser_rd;
    /* read conversion data */
    b = (temp & 0xffff0000) >> 16;
    /* get data b */
    c = (temp & 0xffff) >> 16;
    /* get data c */

    denom[i] = (a*a + b*b + c*c) >> 16;
    adot = a - a_temp;
    /* calculate derivatives */
    bdot = b - b_temp;
    cdot = c - c_temp;
    numer = a*(cdot - bdot) + b*(adot - cdot) + c*(bdot - adot);

    output[i] = DECAy*output[i-1] + numer/denom[i];
    a_temp = a; b_temp = b; c_temp = c;
}
stop = uclock();
printf("\nstart time = %i", start);
printf("\nstop time = %i", stop);
printf("\ntime taken = %i", (stop - start) );
}

```

H. PROGRAM TST3.ASM

```
.title "Data sampling using Mux"
*****
*
* TST3.ASM - Routine to take data from DSP102 at Max
* sampling rate using Multiplexed input on input A of DSP102.
* Data is stored in vectors a_dat, b_dat and c_dat.
* fs = 75,757.6 Hz
*
*****
*
* Reset and interrupt vector table specification. This
* arrangement assumes that during linking, the following
* text segment will be placed to start at the origin of the
* vector table.
*

.global reset,start
.global rint0,int06,XRPT

reset .sect "MC_vec" ; Named section
* .word start ; Hardware reset vector

.word XRPT ; EI0 (01)
.word XRPT ; EI1 (02)
.word XRPT ; EI2 (03)
.word XRPT ; EI3 (04)

rint0 .word XRPT ; Serial port 0 XMT (05)
.word int06 ; Serial port 0 RCV (06)

.word XRPT ; Serial port 1 XMT (07)
.word XRPT ; Serial port 1 RCV (08)

.word XRPT ; Timer 0 (09)
.word XRPT ; Timer 1 (10)

.word XRPT ; DMA (11)

.space 20 ; Reserved

.space 32 ; Space for the 32 traps (32-63)

*
* Entry point for TST3 routine
* Initialization routine
*
;
; constants for initialization routines
```

```

.data
base .word 00808000h ; base address of onchip peripherals
ser_ini .word 0ebc0040h ; serial data bus initialization word
ser_gc .word 00808040h ; base address of serial port 0
ser_rd .word 0080804ch ; address of serial port receive data
stack .word 00809810h ; address of start of stack
blk0 .word 00809800h ; start address of internal RAM block 0
blk1 .word 00809c00h ; start address of internal RAM block 1

```

```

.text

```

```

; Reconfigure Primary Bus Control Register for PC31

```

```

start LDI @base,AR0 ; Load AR0 with base addr
LDI 1090h,R1 ; Init PBCR for SWW=2,
STI R1,*+AR0(64h) ; and WTCNT = 4.

```

```

;
; intilaize serial port 0

```

```

LDI @ser_ini,R0 ; setup for serial port transfers
STI R0,*+AR0(40h) ; with DSP102 at 8.33333 Mhz
LDI 111h,R0 ; 32 bit words the first 16 MSB bits
STI R0,*+AR0(42h) ; are data A and the 16 LSB bits are B
STI R0,*+AR0(43h)
LDI 0fh,R0
STI R0,*+AR0(44h)
LDI 0,R0
STI R0,*+AR0(45h)
STI R0,*+AR0(46h)

```

```

;
; zero internal memory

```

```

LDI @blk0,AR0 ; AR0 points to RAM block 0
LDI @blk1,AR1 ; AR1 points to RAM block 1
LDI 0,R0 ; load intialization value 00
RPTS 1023 ; repeat 1023 times
STI R0,*AR0++(1) ; zero RAM block 0
|| STI R0,*AR1++(1) ; zero RAM block 1

```

```

;
; initialize and start internal timer 1

```

```

LDI @base,AR0 ; base address of on-chip peripherals
STI R0,*+AR0(30h) ; stop timer 1
LDI 55,R0 ; setup count for 151,515.2 Hz
STI R0,*+AR0(38h)
LDI 2c1h,R0 ; setup for 1 cycle pluse
STI R0,*+AR0(30h) ; and start timer 1

```

```

;
; initialize stack pointer

```

```

LDI @stack,SP ; intialize stack pointer
LDI @MUX,AR0 ; load address of Multiplexer
LDI @Mux,AR2 ; load address of mux shadow register
LDI 0,R0
STI R0,*AR0 ; set mux channel IN0
|| STI R0,*AR2 ; update mux shadow reg

```

```

;
; clear first two samples of ADC before starting loop
wait1 LDI    @ser_rd,AR1      ; load address of serial port0 receive
      TSTB   20h,IF          ; wait for serial port interrupt
      BZ     wait1
      LDI    1,R2            ;
      STI    R2,*AR0         ; change mux to channel IN1
      LDI    *AR1,R1         ; dummy read of serial data
      STI    R1,@dummy1      ; store at dummy1
      XOR    IF,IF           ; clear interrupt flag
wait2 TSTB   20h,IF          ; wait for next interrupt
      BZ     wait2
      STI    R0,*AR0         ; change mux back to channel IN0
      LDI    *AR0,R1         ; dummy read
      STI    R1,@dummy2      ; store at dummy2
      XOR    IF,IF           ; clear interrupt flag
;
; load registers for the interrupt service routine
      LDP    0               ; load data page to point to bss section
      LDI    @A_dat,AR3      ; AR3 points to data A
      LDI    @B_dat,AR4      ; AR4 points to data B
      LDI    @C_dat,AR5      ; AR5 points to data C
      LDI    @MASK,RC        ; RC has mask value
      LDI    0,IR0           ; zero data index pointer

      LDI    20h,IE          ; enable serial port0 receive interrupt
      LDI    2800h,ST        ; and enable global interrupts and cache
;
; go into infinite loop
loop:  B      loop
;
; Interrupt service routine to read ADC conversion data
int06: IACK   *AR2           ; interrupt acknowledge signal
      LDI    *AR1,R1         ; read data from serial port
      LDI    *AR2,R0         ; check if mux is set to channel IN0
      BNZ    int06a
      ASH    -16,R1          ; store upper 16 MSBs as data A
      BD     int06b          ; return when read
      STI    R1,*+AR3(IR0)   ; and store it away
      LDI    1,R0            ;
      STI    R0,*AR0         ; change mux channel to IN0
||     STI    R0,*AR2         ; update shadow register
int06a LDI    0,R2
      STI    R2,*AR0         ; change mux to channel IN1
||     STI    R2,*AR2         ; update mux shadow register
      LDI    R1,R2
      ASH    -16,R1          ; shift 16 MSBs to the right
      STI    R1,*+AR4(IR0)   ; store B data
      AND    RC,R2           ; mask off lower 16 LSB
      ASH    16,R2           ; rotate 16 bits left to set sign

```



```

        ASH    -16,R2                ; rotate back preserving sign
        STI    R2,*+AR5(IR0)        ; store C data
        ADDI   1,IR0                ; increment data pointer
        CMPI   @SIZE,IR0            ; at end of data buffer yet?
        LDIZ   0,IR0                ; if so set index pointer to start
int06b: IACK   *AR2                  ; interrupt acknowledge
        RETI

```

```

;
; Interrupt service routine for unspecified interrupts
XRPT:

```

```

    RETI

```

```

;
; program data definition

```

```

    .globl    size
    .globl    a,b,c
    .bss      a,2000h
    .bss      b,2000h
    .bss      c,2000h
    .globl    mux
    .bss      mux,1
    .globl    dummy1
    .bss      dummy1,1
    .globl    dummy2
    .bss      dummy2,1

```

```

    .data
MASK .word 0ffffh
SIZE .word 2000h
A_dat .word a
B_dat .word b
C_dat .word c
Mux .word mux
MUX .word 0ffa80h

```

```

    .end

```

I. PROGRAM TST5.ASM

```

        .title    "Multiplexed demodulator using integer math"
        ****
*
* TST5.ASM - Digital demodulation algortihm using integer operations.
*   Input data is sampled at Max rate using Multiplexed inputs
*   on input A of the DSP102. 8192 points of Denominator
*   numerator and output data are stored.
*
        ****
* Reset and interrupt vector table specification. This
* arrangement assumes that during linking, the following
* text segment will be placed to start at the origin of the
* vector table.
*

        .global  reset,start
        .global  rint0,int06,XRPT
        .ref     DIV_I,DIV_U

reset    .sect     "MC_vec"      ; Named section
*        .word     start         ; Hardware reset vector

        .word     XRPT           ; EI0                (01)
        .word     XRPT           ; EI1                (02)
        .word     XRPT           ; EI2                (03)
        .word     XRPT           ; EI3                (04)

rint0    .word     XRPT           ; Serial port 0 XMT    (05)
        .word     int06          ; Serial port 0 RCV    (06)

        .word     XRPT           ; Serial port 1 XMT    (07)
        .word     XRPT           ; Serial port 1 RCV    (08)

        .word     XRPT           ; Timer 0              (09)
        .word     XRPT           ; Timer 1              (10)

        .word     XRPT           ; DMA                  (11)

        .space     20            ; Reserved

        .space     32            ; Space for the 32 traps (32-63)

; Entry point for TST5 routine
; Initialization
;
; constants for intialization routines
        .data
base     .word     00808000h

```

```

ser_ini .word 0ebc0040h      ; serial data bus initialization word
ser_gc  .word 00808040h      ; base address of serial port 0
ser_rd  .word 0080804ch      ; address of received data
stack   .word 00809810h      ; address of start of stack
blk0    .word 00809800h      ; start address of internal RAM block 0
blk1    .word 00809c00h      ; start address of internal RAM block 1

```

```

.text

```

```

; Reconfigure Primary Bus Control Register for PC31
;

```

```

start  LDI    @base,AR0      ; Load AR0 with base addr
        LDI    1090h,R1      ; Init PBCR for SWW=2,
        STI    R1,*+AR0(64h) ; and WTCNT = 4.
;

```

```

; intilaize serial port 0

```

```

        LDI    @ser_ini,R0    ; setup for serial port transfers
        STI    R0,*+AR0(40h)  ; with DSP102 at 8.33333 Mhz
        LDI    111h,R0        ; 32 bit words the first 16 MSB bits
        STI    R0,*+AR0(42h)  ; are data A and the 16 LSB bits are B
        STI    R0,*+AR0(43h)
        LDI    0fh,R0
        STI    R0,*+AR0(44h)
        LDI    0,R0
        STI    R0,*+AR0(45h)
        STI    R0,*+AR0(46h)
;

```

```

; zero internal memory

```

```

        LDI    @blk0,AR0      ; AR0 points to RAM block 0
        LDI    @blk1,AR1      ; AR1 points to RAM block 1
        LDI    0,R0           ; load intialization value 00
        RPTS    1023          ; repeat 1023 times
        STI    R0,*AR0++(1)   ; zero RAM block 0
||      STI    R0,*AR1++(1)   ; zero RAM block 1
;

```

```

; initialize internal timer 1

```

```

        LDI    @base,AR0      ; base address of peripherals
        STI    R0,*+AR0(30h)  ; stop timer 1
        LDI    60,R0          ; setup count for 151.5 Khz
        STI    R0,*+AR0(38h)
        LDI    2c1h,R0        ; setup for 1 cycle pluse
        STI    R0,*+AR0(30h)  ; and start timer 1
;

```

```

; initialize stack pointer and multiplexer

```

```

        LDI    @stack,SP      ; initialize stack pointer
        LDI    @MUX,AR0
        LDI    0,R0
        STI    R0,*AR0        ; set multiplexer to channel IN0
        STI    R0,@mux        ; update mux shadow register
;

```

```

; Clear first two samples from ADC and get initial samples
; for A,B and C to calculate initial first derivatives

```

```

;
LDI @ser_gc,AR1 ; base address of serial port 0
LDI 1,R0
wait1 TSTB R0,*AR1 ; wait for a data conversion
BZ wait1 ; perform 2 dummy reads and then get
LDI *+AR1(0ch),R1 ; initialization data
wait2 TSTB R0,*AR1 ; wait for next conversion
BZ wait2
LDI *+AR1(0ch),R1 ; dummy read of data
wait3 TSTB R0,*AR1 ; wait for another conversion
BZ wait3 ;
LDI *+AR1(0ch),R1 ; read data from serial port 0
STI R0,*AR0 ; change multiplexer to channel IN1
ASH -16,R1 ; get upper 16 MSBs
STI R1,@aprev ; store as previous sample for derivative
wait4 TSTB R0,*AR1 ; wait for next conversion
BZ wait4 ;
LDI *+AR1(0ch),R1 ;
LDI 0,R3 ; switch multiplexer back to IN0
STI R3,*AR0 ;
LDI R1,R2 ; save data temporarily
ASH -16,R1 ; get upper 16 MSBs
LDI R1,R4
STI R1,@bprev ; store B sample for derivative calculation
AND 0ffffh,R2 ; mask off lower 16 LSBs
ASH 16,R2 ;
ASH -16,R2 ; preserve sign of result
STI R2,@cprev ; store C sample for previous value
wait5 TSTB R0,*AR1 ; wait for next conversion
BZ wait5 ;
LDI *+AR1(0ch),R1 ; read data
STI R0,*AR0 ; change mux to channel IN1
ASH -16,R1 ; store A data in R1
STI R1,@asave ; store A at asave
wait6 TSTB R0,*AR1 ; wait for next conversion
BZ wait6 ;
LDI *+AR1(0ch),R0 ;
LDI 0,R2 ;
STI R2,*AR0 ; switch mux back to IN0
LDI R0,R2 ;
ASH -16,R2 ; data B in R2
STI R2,@bsave ; store B data at bsave
AND 0ffffh,R0 ; mask off C data
ASH 16,R0 ; shift left 16 bits to set sign
ASH -16,R0 ; renormalize data, data C in R0
STI R0,@csave ; save data C at csave
LDI @Prev,AR7 ; base address of previous data samples
SUBI *AR7,R1,R3 ; adot = (asave - aprev) adot in R3
STI R3,@adot ; store adot
STI R1,*AR7++ ; update aprev
SUBI *AR7,R2,R4 ; bdot = (bsave - bprev) bdot in R4

```

```

STI    R4,@bdot          ; store bdot
STI    R2,*AR7++         ; update bprev
SUBI   *AR7,R0,R5        ; cdot = (csave - cprev) cdot in R5
STI    R5,@cdot          ; store cdot
STI    R0,*AR7           ; update cprev
MPYI   R1,R1             ; square A data
MPYI   R2,R2             ; square B data
MPYI   R0,R0             ; square C data
ADDI   R0,R2             ; C^2 + B^2
ADDI   R2,R1             ; C^2 + B^2 + A^2  denom in R1
ASH    -16,R1            ; scale denominator by 65536
LDI    @Denom,AR2        ;
STI    R1,*AR2           ; store denominator
SUBI   R3,R4,R2          ; (bdot - abot) save in R2
MPYI   R2,*AR7--,R2      ; numer3 = c*(bdot - adot) in R2
ASH    -1,R2             ; divide numer3 by 2
SUBI   R5,R3,R6          ; (adot - cdot) save in R6
MPYI   R6,*AR7--,R6      ; numer2 = b*(adot - cdot) in R6
ASH    -1,R6             ; divide numer2 by 2
SUBI   R4,R5,R0          ; (cdot - bdot) save in R0
MPYI   R0,*AR7,R0        ; numer1 = a*(cdot - bdot) in R0
ASH    -1,R0             ; divide numer1 by 2
ADDI   R2,R6             ; numer2 + numer3
ADDI   R6,R0             ; numer=numer1+numer2+numer3 in R0
LDI    @Numer,AR2        ; base address of numerator data
STI    R0,*AR2           ; store numerator data
CALL   DIV_I             ; Divide R0/R1
LDI    @Output,AR2       ; load base address of output
STI    R0,@last          ; initialize last output value
STI    R0,*AR2           ; store at first output value
; load registers for the interrupt service routine
;
LDP    0                 ; load data page to point to bss section
LDI    @MUX,AR0           ; AR0 has address of multiplexer
LDI    @ser_rd,AR1        ; AR1 has address of serial read data
LDI    @Mux,AR2           ; AR2 has address of mux shadow reg
LDI    @Denom,AR3         ; AR3 points to denominator data
LDI    @Numer,AR4         ; AR4 points to numerator data
LDI    @Output,AR5        ; AR5 points to output data
LDI    @MASK,BK           ; BK has mask value
LDI    1,IR0             ; zero data index pointer

LDI    20h,IE            ; enable serial port0 receive interrupt
LDI    2800h,ST          ; and enable global interrupts and cache
; go into infinite loop
;
loop:   B      loop
;
; serial port 0 interrupt service routine
int06: LDI    2800h,ST    ; reenale interrupts

```

	LDI	*AR1,RS	; read data from serial port 0
	LDI	*AR2,R7	; check mux shadow reg
	BNZ	int06a	;
	ASH	-16,RS	; mask off LSB 16 bits
	BD	int06b	;
	STI	RS,@asave	; store A data at asave
	LDI	1,R7	;
	STI	R7,*AR0	; change mux to IN0
	STI	R7,*AR2	; update mux shadow reg
int06a	LDI	0,R1	;
	STI	R1,*AR0	; change mux to IN1
	STI	R1,*AR2	; update mux shadow register
	LDI	RS,R1	;
	ASH	-16,R1	;
	LDI	R1,R4	; save data B in R4
	MPYI	R1,R1	; save B^2 in R1
	AND	BK,RS,R2	; mask off C data
	ASH	16,R2	; shift left 16 bits to set sign
	ASH	-16,R2	; renormalize data
	LDI	R2,R5	; save data C in R5
	MPYI	R2,R2	; save c^2 in R2
	LDI	@asave,R3	; restore data A
	LDI	R3,R6	; save data A in R6
	MPYI	R3,R3	; save a^2 in R3
	ADDI	R3,R1	; (a^2 + b^2)
	ADDI	R2,R1	; (a^2 + b^2 + c^2)
	ASH	-16,R1	; divide denominator by 2^16
	STI	R1,*+AR3(IR0)	; store and keep denominator in R1
	LDI	@Prev,AR7	; base address of previous data samples
	SUBI	*AR7,R6,R0	; adot = (asave - aprev) adot in R0
	STI	R6,*AR7++	; update aprev
	SUBI	*AR7,R4,R2	; bdot = (bsave - bprev) bdot in R2
	STI	R4,*AR7++	; update bprev
	SUBI	*AR7,R5,R3	; cdot = (csave - cprev) cdot in R3
	STI	R5,*AR7	; update cprev
	SUBI	R0,R2,R4	; (bdot - abot) save in R4
	MPYI	R4,*AR7--,R4	; numer3 = c*(bdot - adot) in R4
	ASH	-1,R4	; divide numer1 by 2
	SUBI	R3,R0,R5	; (adot - cdot) save in R5
	MPYI	R5,*AR7--,R5	; numer2 = b*(adot - cdot) in R5
	ASH	-1,R5	; divide numer2 by 2
	SUBI	R2,R3,R6	; (cdot - bdot) save in R6
	MPYI	R6,*AR7,R6	; numer1 = a*(cdot - bdot) in R6
	ASH	-1,R6	; divide numer3 by 2
	ADDI	R5,R6	; numer2 + numer3
	ADDI	R6,R4,R0	; numer=numer1+numer2+numer3 in R0
	LDI	@Numer,AR4	; base address of numerator data
	STI	R0,*+AR4(IR0)	; store numerator data
	CALL	DIV_I	; Divide R0/R1
	FLOAT	R0	; convert to floating point
	LDI	@last,R1	; load previous output

```

        FLOAT R1                ; convert to floating point
        MPYF  @DECAY,R1        ; Multiply decay*last output
        ADDF  R1,R0
        FIX   R0,R2
        LDI   @Output,AR5      ; get pointer to output data
        STI   R2,*+AR5(IR0)    ; store output
        STI   R2,@last         ; update last output value
        ADDI  1,IR0            ; increment data pointer
        CMPI  @SIZE,IR0        ; at end of data buffer yet?
        LDIZ  0,IE             ; if so disable interrupts
int06b:
        RETI

```

```

; Interrupt service routine for unspecified interrupts
;

```

```

XRPT:
        RETI
;

```

```

; system data definitions

```

```

        .globl  denom
        .bss    denom,2000h
        .globl  numer
        .bss    numer,2000h
        .globl  output
        .bss    output,2000h
        .globl  asave,bsave,csave
        .bss    asave,1
        .bss    bsave,1
        .bss    csave,1
        .globl  aprev
        .bss    aprev,1
        .globl  bprev
        .bss    bprev,1
        .globl  cprev
        .bss    cprev,1
        .globl  last
        .bss    last,1
        .globl  mux
        .bss    mux,1
        .globl  adot,bdot,cdot
        .bss    adot,1
        .bss    bdot,1
        .bss    cdot,1

```

```

        .data
MASK    .word  0ffffh
DECAY    .float 9.9e-1
SIZE     .word  2000h
Denom    .word  denom
Numer    .word  numer
Output   .word  output

```

```
MUX .word 0ffa80h
Mux .word mux
Prev .word aprev
Save .word asave
.end
```


J. PROGRAM TST7.ASM

```

        .title    "Multiplexed demodulator using floating point"
*****
*
* TST7.ASM - Demodulation routine taking data from DSP102
*   at Max sampling rate using Multiplexed inputs. Demodulation
*   is done using floating point operations. 8192 (decimal) points of the
*   denominator, numerator and output signals are computed and stored.
*
*****
* Reset and interrupt vector table specification. This
* arrangement assumes that during linking, the following
* text segment will be placed to start at the origin of the
* vector table.
*

        .global  reset,start
        .global  rint0,int06,XRPT
        .ref     DIV_F

reset    .sect     "MC_vec"      ; Named section
*        .word     start         ; Hardware reset vector

        .word     XRPT          ; EI0                (01)
        .word     XRPT          ; EI1                (02)
        .word     XRPT          ; EI2                (03)
        .word     XRPT          ; EI3                (04)

rint0    word      XRPT          ; Serial port 0 XMT      (05)
        word      int06         ; Serial port 0 RCV      (06)

        .word     XRPT          ; Serial port 1 XMT      (07)
        .word     XRPT          ; Serial port 1 RCV      (08)

        .word     XRPT          ; Timer 0                (09)
        .word     XRPT          ; Timer 1                (10)

        .word     XRPT          ; DMA                    (11)

        .space     20           ; Reserved

        .space     32           ; Space for the 32 traps (32-63)

; Entry point for TST7 routine
; Initialization
;
; constants for initialization routines
        .data
base     .word     00808000h      ; base address of onboard peripherals

```

```

ser_ini .word 0ebc0040h      ; serial data bus initialization word
ser_gc  .word 00808040h      ; base address of serial port 0
ser_rd  .word 0080804ch      ; address of received data
stack   .word 00809810h      ; address of start of stack
blk0    .word 00809800h      ; start address of internal RAM block 0
blk1    .word 00809c00h      ; start address of internal RAM block 1

```

```

.text
; Reconfigure Primary Bus Control Register for PC31
;
start  LDI    @base,AR0      ; Load AR0 with base addr
        LDI    1090h,R1      ; Init PBCR for SWW=2,
        STI    R1,*+AR0(64h) ; and WTCNT = 4.
;
; intilaize serial port 0
;
        LDI    @ser_ini,R0   ; setup for serial port transfers
        STI    R0,*+AR0(40h) ; with DSP102 at 8.33333 Mhz
        LDI    111h,R0       ; 32 bit words the first 16 MSB bits
        STI    R0,*+AR0(42h) ; are data A and the 16 LSB bits are B
        STI    R0,*+AR0(43h)
        LDI    0fh,R0
        STI    R0,*+AR0(44h)
        LDI    0,R0
        STI    R0,*+AR0(45h)
        STI    R0,*+AR0(46h)
;
; zero internal memory
        LDI    @blk0,AR0     ; AR0 points to RAM block 0
        LDI    @blk1,AR1     ; AR1 points to RAM block 1
        LDI    0,R0           ; load intialization value 00
        RPTS    1023          ; repeat 1023 times
        STI    R0,*AR0++(1)   ; zero RAM block 0
||      STI    R0,*AR1++(1)   ; zero RAM block 1
;
; initialize internal timer 1
        LDI    @base,AR0     ; base address of peripherals
        STI    R0,*+AR0(30h) ; stop timer 1
        LDI    55,R0          ; setup count for 151,515.2 Hz
        STI    R0,*+AR0(38h)
        LDI    2c1h,R0        ; setup for 1 cycle pluse
        STI    R0,*+AR0(30h) ; and start timer 1
;
; initialize stack pointer and multiplexer
        LDI    @stack,SP      ; initialize stack pointer
        LDI    @MUX,AR2       ;
        LDI    0,R0           ;
        STI    R0,*AR2         ; set multiplexer to channel IN0
        STI    R0,@mux        ; update mux shadow register
;
; Clear first two samples from ADC and get values to

```

```

; initialize first computations
;
LDI    @ser_gc,AR1    ; base address of serial port 0
LDI    1,R0
wait1  TSTB R0,*AR1    ; wait for a data conversion
      BZ    wait1      ; perform 2 dummy reads and then get
      LDI    *+AR1(0ch),R1 ; initialization data
wait2  TSTB R0,*AR1    ; wait for next conversion
      BZ    wait2
      LDI    *+AR1(0ch),R1 ; dummy read of data
wait3  TSTB R0,*AR1    ; wait for another conversion
      BZ    wait3      ;
      LDI    *+AR1(0ch),R1 ; read data from serial port 0
      STI    R0,*AR2      ; change multiplexer to channel IN1
      ASH    -16,R1        ; get upper 16 MSBs
      FLOAT R1
      STF    R1,@aprev    ; store as previous sample for derivative
wait4  TSTB R0,*AR1    ; wait for next conversion
      BZ    wait4      ;
      LDI    *+AR1(0ch),R1 ;
      LDI    0,R3        ; switch multiplexer back to IN0
      STI    R3,*AR2      ;
      LDI    R1,R2        ; save data temporarily
      ASH    -16,R1        ; get upper 16 MSBs
      FLOAT R1            ; convert to floating pt
      STF    R1,@bprev    ; store B sample for derivative calculation
      AND    0ffffh,R2    ; mask off lower 16 LSBs
      ASH    16,R2        ;
      ASH    -16,R2        ; preserve sign of result
      FLOAT R2            ; convert to floating pt
      STF    R2,@cprev    ; store C sample for previous value
wait5  TSTB R0,*AR1    ; wait for next conversion
      BZ    wait5      ;
      LDI    *+AR1(0ch),R1 ; read data
      STI    R0,*AR2      ; change mux to channel IN1
      ASH    -16,R1        ; store A data in R1
      FLOAT R1            ; convert data to floating pt
wait6  TSTB R0,*AR1    ; wait for next conversion
      BZ    wait6      ;
      LDI    *+AR1(0ch),R0 ;
      LDI    0,R2        ;
      STI    R2,*AR2      ; switch mux back to IN0
      LDI    R0,R2        ;
      ASH    -16,R2        ; data B in R2
      FLOAT R2            ; convert data B to floating pt
      AND    0ffffh,R0    ; mask off C data
      ASH    16,R0        ; shift left 16 bits to set sign
      ASH    -16,R0        ; renormalize data, data C in R0
      FLOAT R0            ; convert data C to floating pt
      LDI    @Prev,AR7    ; base address of previous data samples
      SUBF   *AR7,R1,R3    ; adot = (asave - aprev) adot in R3

```

```

STF    R1,*AR7++      ; update aprev
SUBF   *AR7,R2,R4     ; bdot = (bsave - bprev) bdot in R4
STF    R2,*AR7++      ; update bprev
SUBF   *AR7,R0,R5     ; cdot = (csave - cprev) cdot in R5
STF    R0,*AR7        ; update cprev
MPYF   R1,R1          ; square A data
MPYF   R2,R2          ; square B data
MPYF   R0,R0          ; square C data
ADDF   R0,R2          ; C^2 + B^2
ADDF   R2,R1          ; C^2 + B^2 + A^2  denom in R1
SUBF   R3,R4,R2       ; (bdot - abot) save in R2
MPYF   R2,*AR7--,R2   ; numer3 = c*(bdot - adot) in R2
SUBF   R5,R3,R6       ; (adot - cdot) save in R6
MPYF   R6,*AR7--,R6   ; numer2 = b*(adot - cdot) in R6
SUBF   R4,R5,R0       ; (cdot - bdot) save in R0
MPYF   R0,*AR7,R0     ; numer1 = a*(cdot - bdot) in R0
ADDF   R2,R6          ; numer2 + numer3
ADDF   R6,R0          ; numer=numer1+numer2+numer3 in R0
CALL   DIV_F          ; Divide R0/R1
STF    R0,@last       ; initialize last output value
LDI    @Output,AR2    ; load base address of output
MPYF   @SCALE,R0      ; scale output before conversion to int
FIX    R0             ; convert output to integer
STI    R0,*AR2        ; store at first output value
;
; load registers for the interrupt service routine
;
LDP    0              ; load data page to point to bss section
LDI    @MUX,AR0       ; AR0 has address of multiplexer
LDI    @ser_rd,AR1    ; AR1 has address of serial read data
LDI    @Mux,AR2       ; AR2 has address of mux shadow reg
LDI    @Output,AR3    ; AR5 points to output data
LDI    @MASK,BK       ; BK has mask value
LDI    1,IR0          ; zero data index pointer

LDI    20h,IE         ; enable serial port0 receive interrupt
LDI    2800h,ST       ; and enable global interrupts and cache
;
; go into infinite loop
;
loop:   B      loop
;
; serial port 0 interrupt service routine
int06: LDI    2800h,ST ; reenale interrupts
LDI    *AR1,RS        ; read data from serial port 0
LDI    *AR2,R7        ; check mux shadow reg
BNZ    int06a         ;
ASH    -16,RS         ; mask off LSB 16 bits
FLOAT  RS,R7
BD     int06b         ;

```

```

    STF    R7,@asave      ; store A data at asave
    LDI    1,R7           ;
    STI    R7,*AR0        ; change mux to IN0
||  STI    R7,*AR2        ; update mux shadow reg
int06a: LDI    0,R1       ;
    STI    R1,*AR0        ; change mux to IN1
||  STI    R1,*AR2        ; update mux shadow register
    LDI    RS,R1          ;
    ASH    -16,R1         ;
    FLOAT  R1             ;
    LDF    R1,R4          ; save data B in R4
    MPYF   R1,R1          ; save B^2 in R1
    AND    BK,RS,R2       ; mask off C data
    ASH    16,R2          ; shift left 16 bits to set sign
    ASH    -16,R2         ; renormalize data
    FLOAT  R2             ;
    LDF    R2,R5          ; save data C in R5
    MPYF   R2,R2          ; save c^2 in R2
    LDF    @asave,R3      ; restore data A
    LDF    R3,R6          ; save data A in R6
    MPYF   R3,R3          ; save a^2 in R3
    ADDF   R3,R1          ; (a^2 + b^2)
    ADDF   R2,R1          ; (a^2 + b^2 + c^2)
    LDI    @Prev,AR7      ; base address of previous data samples
    SUBF   *AR7,R6,R0     ; adot = (asave - aprev) adot in R0
    STF    R6,*AR7++      ; update aprev
    SUBF   *AR7,R4,R2     ; bdot = (bsave - bprev) bdot in R2
    STF    R4,*AR7++      ; update bprev
    SUBF   *AR7,R5,R3     ; cdot = (csave - cprev) cdot in R3
    STF    R5,*AR7        ; update cprev
    SUBF   R0,R2,R4       ; (bdot - adot) save in R4
    MPYF   R4,*AR7--,R4   ; numer3 = c*(bdot - adot) in R4
    SUBF   R3,R0,R5       ; (adot - cdot) save in R5
    MPYF   R5,*AR7--,R5   ; numer2 = b*(adot - cdot) in R5
    SUBF   R2,R3,R6       ; (cdot - bdot) save in R6
    MPYF   R6,*AR7,R6     ; numer1 = a*(cdot - bdot) in R6
    ADDF   R5,R6          ; numer2 + numer3
    ADDF   R6,R4,R0       ; numer=numer1+numer2+numer3 in R0
    CALL   DIV_F          ; Divide R0/R1
    LDF    @last,R1       ; load previous output
    MPYF   @DECAY,R1      ; Multiply decay*last output
    ADDF   R1,R0          ;
    STF    R0,@last       ; update last output sample
    MPYF   @SCALE,R0      ; scale output for integer value
    FIX    R0             ; convert to integer
    STI    R0,*+AR3(IR0)  ; store integer output
    ADDI   1,IR0          ; increment data pointer
    CMPI   @SIZE,IR0      ; at end of data buffer yet?
    LDIZ   0,IE           ; if so disable interrupts
int06b: RETI

```

; Interrupt service routine for unspecified interrupts

;

XRPT:

RETI

;

; system data definitions

.globl denom
.bss denom,2000h
.globl numer
.bss numer,2000h
.globl output
.bss output,2000h
.globl asave
.bss asave,1
.globl aprev
.bss aprev,1
.globl bprev
.bss bprev,1
.globl cprev
.bss cprev,1
.globl last
.bss last,1
.globl mux
.bss mux,1

.data

MASK .word 0ffffh
DECAY .float 9.9e-1
SIZE .word 2000h
SCALE .float 30000.0
Denom .word denom
Numer .word numer
Output .word output
MUX .word 0ffa80h
Mux .word mux
Prev .word prev
Save .word save

.end

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